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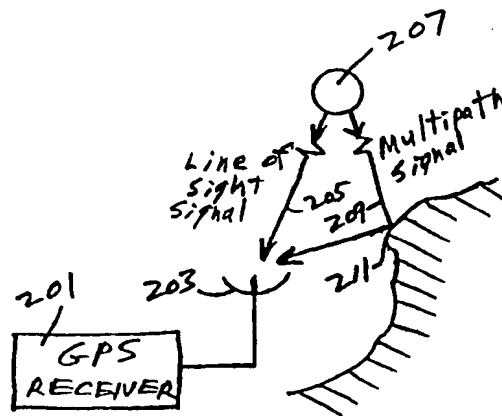
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(54) Title: MULTIPATH ERROR REDUCTION IN A SPREAD SPECTRUM RECEIVER FOR RANGING APPLICATIONS

(57) Abstract

A receiver of a radio frequency signal having a pseudo-random noise (PRN) code, and techniques of processing such a signal that are especially adapted for ranging applications. A signal corresponding to the PRN code is locally generated and used for decoding the received signal in a manner to reduce ranging errors that can result when multipath (delayed) versions of the radio frequency signal are also present. A significant application of the receiver and signal processing techniques of the present invention is in a Global Positioning System (GPS), wherein a number of such signals from several satellites are simultaneously received and processed in order to obtain information of the position, movement, or the like, of the receiver. A delay locked loop (DLL) correlator, provided in each of the receiver's multiple processing channels, locks onto a line of sight signal from one of the satellites with the effect of any multipath signal(s) being significantly reduced.



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MULTIPATH ERROR REDUCTION IN A SPREAD SPECTRUM RECEIVER
FOR RANGING APPLICATIONS

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Background of the Invention

10 This invention relates to digital radio
receivers which are used for navigation systems and
other ranging applications, wherein the received signals
are encoded with a pseudo-random noise (PRN) type code.
This invention deals specially with environments where
15 the multipath fading is severe.

 The United States government has placed into
orbit a number of satellites as part of a global
positioning system (GPS). A GPS receiver receives
signals from several such satellites and can determine
20 very accurate parameters, such as position, velocity,
and time. There are both military and commercial uses.
A primary military use is for a receiver in an aircraft
or ship to constantly determine the position and
velocity of the plane or ship. An example of a
25 commercial use includes surveying and the accurate
determination of the location of a fixed point or a
distance between two fixed points, with a high degree of
accuracy. Another example is the generation of a high
accuracy timing reference.

30 In order to accomplish this, each satellite
continually transmits two L-band signals. A receiver
simultaneously detects the signals from several
satellites and processes them to extract information
from the signals in order to calculate the desired

parameters, such as position, velocity or time. The United States government has adopted standards for these satellite transmissions so that others may utilize the satellite signals by building receivers for specific purposes. The satellite transmission standards are set forth in detail by an "Interface Control Document" of Rockwell International Corporation, entitled "Navstar GPS Space Segment/Navigation User Interfaces", dated September 26, 1984, as revised December 19, 1986.

Briefly, each satellite transmits an L1 signal on a 1575.42Mhz carrier, usually expressed as $1540f_0$, where $f_0=1.023\text{Mhz}$. A second, L2 signal transmitted by each satellite, has a carrier frequency of 1227.6 Mhz, or $1200f_0$. Each of these signals is modulated in the satellite by at least one pseudo-random signal function that is unique to that satellite. This results in developing a spread spectrum signal that resists radio frequency noise or intentional jamming. It also allows the L-band signals from a number of satellites to be individually identified and separated in a receiver. One such pseudo-random function is a precision code ("P-code") that modulates both of the L1 and L2 carriers in the satellite. The P-code has a 10.23Mhz clock rate and thus causes the L1 and L2 signals to have a 20.46Mhz bandwidth. The length of the code is seven days; that is, the P-code pattern is begun again every seven days. In addition, the L1 signal of each satellite is modulated by a second pseudo-random function, or a unique clear acquisition code ("C/A code"), having a 1.023Mhz clock rate and repeating its pattern every one millisecond, thus containing 1023 bits. Further, the L1 carrier is also modulated by a 50 bit-per-second navigational data stream that provides certain information of satellite identification, status and the like.

In a receiver, in the process of demodulating those satellite signals, signals corresponding to the known pseudo-random functions are generated and aligned in phase with those modulated onto the satellite signals. The phase of the carriers from each satellite being tracked is measured from the results of correlating each satellite signal with a locally generated pseudo-random function. The relative phase of carrier signals from a number of satellites is a measurement that is used by a receiver to calculate the desired end quantities of distance, velocity, time, etc. Since the P-code encrypted functions (Y-code) are to be classified by the United States government so that they can be used for military purposes only, commercial users of the GPS must work directly only with the C/A code pseudo-random function.

The government of the former USSR has placed into orbit a similar satellite positioning system called GLONASS; more information on its standard can be found in the "Global Satellite Navigation System GLONASS-Interface Control Document" of the RTCA Paper No. 518-91/SC159-317, approved by the Glavkosmos Institute of Space Device Engineering, the official former USSR GLONASS responsible organization. Although the present invention is described herein for use with the United States GPS system, it can be applied to a receiver designed to acquire the GLONASS signals or any radio frequency system using pseudo-random noise sequences for ranging.

One of the major factors influencing the final accuracy of a distance, velocity, etc., measurement being made is the accuracy with which the signal phase measurements are made. In turn, this phase measurement precision is altered if, in addition to the direct line-of-sight propagation signal, a multipath fading signal is also received. The phase of the C/A code, for

example, is determined by use of a delay locked loop (DLL) correlator, wherein the phase of the internally generated C/A PRN code sequence is adjusted in a control loop to minimize an error signal. The DLL uses early
5 and late versions of the internally generated code in a signal correlator that is part of it. Many such receivers use a time spacing between the early and late versions of one PRN code chip. (A "chip" is the time during which the code remains at a plus or minus one.)
10 Operation of the DLL within such receivers is affected by any multipath signal present, thus causing a tracking error. The phase locked condition of the DLL is not only controlled by the line-of-sight signal, as is desired in order to eliminate a cause of phase
15 measurement errors, but rather is affected by the multipath signals as well.

Errors caused by multipath distortion in the out-of-phase condition can be reduced by narrowing the delay spacing between the early and late correlators in
20 the DLL. Although this technique reduces the effect of the received multipath signals somewhat by reducing the loop gain to the weaker multipath signals, inaccuracies still result. The tracking error is never completely eliminated by simply narrowing the early-late delay
25 spacing, no matter what delay in a multipath signal exists.

Therefore, it is a primary and general object of the present invention to further reduce, and even, in some cases, eliminate phase measurement errors that
30 result when one or more multipath versions of a PRN encoded signal are present.

Summary of the Invention

This and additional objects of the present invention are realized, briefly and generally, by
35 providing a DLL correlator having a zero loop gain over

a majority of a range of relative phase difference between the locally generated PRN code and that encoded in the radio frequency signal being received from a satellite or other source, while, at the same time, providing a finite magnitude of loop gain in an operating phase difference region positioned about a zero phase difference. That is, the DLL operates to minimize the error signal for a received signal having a relative phase within a narrow operating phase window and is thus unaffected by multipath versions of that signal which are outside of the window in a region where the loop gain is zero. The present invention exhibits a code loop error which goes practically to zero for far multipath delay, virtually eliminating the influence of the far multipath on the pseudorange measurement accuracy. This improvement is not obtained at the expense of the performances on near multipath, however, in which case the performance is similar to that of the narrow correlator.

In one form of the invention, the radio frequency signal is initially acquired by operating the DLL as a narrow correlator, where there is some gain over the entire range of relative phase differences. After the signal has been acquired by locking the DLL onto a combination of the line-of-sight and multipath signals, the DLL is switched to provide a loop gain in only the small central region, thereby discriminating against the multipath signals.

According to one specific aspect of the present invention, this DLL response is obtained by providing more than one early-late correlator in parallel, with the early-late delays being different. The results of the correlations are arithmetically combined. The size of the central relative phase operating range of the loop response is set by the specific early-late delay values chosen for the

correlators. In the embodiment described hereinafter, two correlators are used, one correlator having an early-late delay of 0.1 chip and the other correlator having a delay of 0.05 chip. During an initial acquisition of the radio frequency signal, only the wider early-late correlator is used.

According to another specific aspect of the present invention, the desired DLL responses are obtained by using specific gating signals in combination with an accumulator/integrator, rather than using early-late versions of the locally generated PRN code. These gating signals are significantly less than one chip in duration and, when in phase with the incoming signal code, occur at each transition of that code between its plus one and negative one values. The gating signals have equal positive and negative areas and have a positive or negative polarity at a center that designates whether the PRN code transition that it represents is positive or negative going. During initial acquisition of the radio frequency signal, the gating signals are shaped as simple positive or negative going pulses occurring at code transitions.

Additional objects, advantages and features of the various aspects of the present invention will become apparent from the following description of its preferred embodiments, which description should be taken in conjunction with the accompanying drawings.

Brief Description of the Drawings

Figure 1 illustrates line-of-sight and multipath signals being received simultaneously by a GPS receiver;

Figures 2 and 3 show the line-of-sight and multipath signals in vector form;

Figure 4 is a general block diagram of a delay locked loop (DLL) correlator;

Figures 5A-5D are curves showing one operation of the circuit of Figure 4;

Figures 6A-6C are curves showing another operation of the circuit of Figure 4;

5 Figures 7 and 8 are block diagrams showing other DLL circuits that are alternatives to that of Figure 4;

Figures 9A-9D are curves which illustrate operation of the DLL circuits of Figures 7 and 8;

10 Figure 10 generally illustrates another type of correlator which uses gating signals for local code generation;

Figures 11A-11D illustrate several ways of operating the circuit of Figure 10;

15 Figure 12 is an enlarged version of a portion of Figure 11D;

Figure 13 shows the results of operating the DLL correlators of Figures 7, 8 and 12 in three different ways;

20 Figure 14 is a block diagram of a complete receiver embodying the various aspects of the present invention;

Figure 15 is a block diagram of the down converter circuit of the receiver of Figure 14, along with timing reference circuitry and sampling;

25 Figure 16 is a block diagram of one channel of the receiver of Figure 14;

Figure 17 shows a carrier numerically controlled oscillator used in each of the channels of Figure 15 in the receiver of Figure 14;

30 Figure 18 shows the PRN code generator of the channel of Figure 16, along with its numerically controlled oscillator;

Figure 19 is a block diagram of the punctual correlator used in the channel circuit of Figure 16;

35

Figure 20 is a block diagram of the DLL correlator (in-phase and quadrature phase) used in the channel circuit of Figure 16; and

Figures 21A-21D illustrate alternate gating signals that may be generated in the circuit of Figure 10.

Description of the Preferred Embodiments

Referring to Figure 1, the various aspects of the present invention are described with respect to a global positioning system (GPS). A GPS receiver 201 includes an antenna 203 which is positioned to receive a signal 205 from a satellite 207. In addition to the desired line-of-sight signal 205 received directly from the satellite 207, the antenna 203 also receives a second version of that signal, a delayed multipath signal 209. The multipath signal is delayed because it reaches the antenna 203 by traversing a longer distance than does the line-of-sight signal 205. The multipath signal is shown in Figure 1 to reflect off of a hill 211, or some other object. Although the present invention is explained simply with reference to a single multipath signal, there can be several delayed versions of the line-of-sight signal which are also received by the antenna 203 at the same time. Since GPS receivers, and other ranging receivers used in other applications, operate by measuring the phase of the received signal, a multipath signal can complicate that task considerably.

Various attempts have been made in antenna design to limit the acceptance of reflected signals. This is difficult, however, because it is generally desired to have the antennas maintain a wide angle property in order to receive signals from several satellites at one time that are spread a considerable distance apart. Attempts have also been made to

position the antenna as high as possible, in order to minimize ground and building reflections, or to carefully position it to avoid receiving reflected signals. Although these techniques may be used in
5 conjunction with the present invention, the present invention uses various signal processing techniques within the receiver itself to discriminate against the received multipath signals.

Referring to Figures 2 and 3, a vector 213
10 represents the received line-of-sight signal, while another vector 215 represents the received multipath signal. The multipath signal 215 arrives at the receiver antenna 203 with a delay τ relative to the line-of-sight signal 213. It is shown in these figures,
15 the multipath signal generally has a lower magnitude than does the line of sight signal as illustrated by its smaller vector 215. A ratio of these magnitudes is noted herein by α .

A delay lock loop (DLL) correlator that is
20 typically used in GPS receivers is shown in Figure 4. A received signal 217 may be radio frequency signal acquired by the antenna 203, after some amplification, but generally is an intermediate frequency signal in a frequency range much lower than that received by the
25 antenna 203. Further, in the GPS receiver environment, a separate such DLL correlator is provided for each satellite signal that is received by the receiver antenna in a single composite signal. One DLL correlator then processes that portion of the incoming
30 signal that emanates from a particular satellite. Further, the signal processing illustrated in Figure 4 is generally done in the digital domain, an analog-to-converter being employed to digitize the incoming intermediate frequency signal. That signal is digitized
35 by a very high frequency sampling clock.

The received signal 217, in whatever form, is mixed in a mixer 219 with a signal 221 that is a replica of the carrier of the received signal 217. This local carrier is generated by an appropriate circuit 223, the phase of the local carrier signal 221 being adjusted by an input control signal 225. A loop circuit to lock the carrier generator 223 onto that of the received signal is not shown in Figure 4 since it can be of a typical design. However, the processing of a signal 227 at an output of the mixer 219 is shown in more detail since it is in this processing where the present invention primarily lies. The signal 227 is the received signal but with its carrier now removed. It is supplied to two mixers 229 and 231 which receive replicas 228 and 230 of a PRN code carried by the received signal. These replicas are, respectively, "early" and "late" in relative phase with respect to a "punctual" replica 245. These replicas come from a local code generator 233 within the receiver. In at least the case of the C/A code in the GPS system, the code carried by the received signal is well known and can be generated within the receivers. The relative phase of the locally generated code is adjusted by a phase control signal 235. Further, in some receivers, another input 237 to the local code generator 233 allows adjustment of the delay between an early and late replicas of the locally generated code.

Outputs of each of the mixers 229 and 231 are applied to appropriate accumulators/integrators 239 and 241, respectively. The outputs of the accumulators 239 and 241 are arithmetically combined in another mixture 243, whose output is an error signal that is applied to the input 235 of the local code generator 233 to adjust its phase. What the loop of Figure 4 is designed to do is to lock the local code generator 233 in phase with the code carried by the received signal 217. Although

this is being described with respect to the C/A code carried by the L1 signals of GPS satellites, the same principles are applicable in a wide variety of applications, particularly in other ranging applications.

It is helpful to refer to the curves of Figures 5A-5D to understand the operation of the DLL correlator of Figure 4. If the punctual output 245 of the local code generator 233 were to be applied to an accumulator of the type of accumulator/integrator 239 or 241, an output characteristic as shown in Figure 5A would result. If this punctual code replica is exactly in phase with the PRN code of the received signal 217, an output of such an accumulator would be a maximum at a center line 247 of the triangular shape output characteristic of Figure 5A. If there is some misalignment in phase between the two, the output of such an accumulator would decrease from such a peak as it travelled down one side or the other of the triangle depending upon whether the local punctual code being generated was delayed or advanced with respect to the PRN code of the received signal.

Although the punctual output of the local code generator 233 is usually used for other purposes in a GPS receiver, the DLL correlator of Figure 4 operates with the early and late versions 228 and 230 of that code. Figure 5B shows the characteristic output of the accumulator 239 from a comparison with the local early code, and the curve of Figure 5C the output function of the accumulator 241 from a comparison with the local late code. In this typical example, the early and late locally generated PRN codes are separated by one chip. That is, the late code 230 is delayed behind the early signal 228 one PRN chip. This fixed delay is designated herein as "d" and is shown in Figure 5B. To state it another way, as shown in relative phase scale along the

x-axis of Figure 5B, the early code function occurs one half a chip in advance of the punctual version, and the late code occurs one half a chip after the punctual version. It is often convenient to reference the early
5 and late correlator outputs, such as shown in Figures 5B and 5C, to a central, in-phase line 247.

Figure 5D shows the error signal 235, resulting from subtracting the correlator function of Figure 5C from that of Figure 5B. The result is a zero
10 error signal at the in-phase point 247 when the local code generator 233 is properly locked onto the PRN code that is part of the received signal 217. As a mismatch in phase occurs, as is well known, the error signal will be driven positive or negative along the curve of Figure
15 5D. Such an error signal drives the phase of the local code generator 233 in a direction to minimize the error signal, thus keeping the local generator 233 locked onto the incoming signal.

However, if one or more multipath signals are
20 received in addition to the desired line-of-sight signal, the DLL correlator of Figure 4 is influenced by both. This is illustrated in Figure 5D. If only the line-of-sight signal 213 existed, the circuit of Figure 4 would cause it to be aligned with the central zero
25 phase reference line 247. However, because of the multipath signal 215 being received, the local code generator 233 "locks" on a fictitious signal having a phase somewhere around them, as shown in Figure 5D. That is, the circuit of Figure 4 is locking on to an
30 incoming code phase that lies somewhere between that of the line-of-sight and multipath signals. Even though the magnitude of the multipath signal may be low with respect to that of the line-of-sight signal, because of attenuation from reflections of the multipath signal,
35 its effect can be significant because of the steep curve of Figure 5D. It is a combination of the multipath

signal magnitude and the value of the curve at the point of the arrow 215, that determines the level of effect of the multipath signal on this phase lock operation. The line-of-sight signal vector 213 will operate around the in-phase point 247 from that of the multipath signal vector 215. Thus, since measurements with the GPS receiver are largely dependent upon an accurate measurement of the relative phase at the point of the receiver of the C/A code in the satellite signals, this effect of a multipath signal is quite significant to the accuracy of the ultimate measurement.

It has been suggested by others that, in order to reduce the effect of a multipath signal, the delay between the early and late local codes being generated into the receiver should be reduced considerably. An effect of a delay $d=0.1$ chip is shown in Figures 6A-6C. The output of the early accumulator 239 in this case is shown in Figure 6A. Similarly, an output of the late accumulator 241 of Figure 4 is shown in Figure 6B. The error signal output of the adder-subtractor 243 is shown in Figure 6C. It will be noticed that since the amplitude of the error signal function is considerably reduced, the multipath signal 215 has a significantly reduced effect. As can be seen from Figure 6C, the magnitude of the error signal curve at the relative phase of the multipath signal vector 215 is much less than in the example of Figure 5B. The result is that, in a steady state phase lock state shown in Figure 6C, the line-of-sight signal vector 213 is positioned much closer to a desired phase locked position 247 than is the line-of-sight signal.

However, as can be seen from Figure 6C, the DLL correlator of Figure 4 operating with an early-late local PRN code phase difference of one tenth of one chip, the DLL still has not locked on the line of sight signal. An error ϵ is reduced in Figure 6C from Figure

5D but is not eliminated. The multipath signal has an effect in creating this error and thus reducing the accuracy by which a GPS receiver may achieve. According to one aspect of the present invention, the effect of
5 multipath signals is eliminated under certain circumstances and further reduced under other circumstances, by forming a DLL correlator of the type shown in Figure 7 wherein two early-late correlations are arithmetically combined. Referring to Figure 7, an
10 output 227 of the carrier mixer 219 is applied to two correlators connected in parallel. A first correlator includes mixers 251 and 253, the outputs of which are applied to an adder-subtractor 255. An output of the latter mixer is then applied to an
15 accumulator/integrator 257. Similarly, the second correlator includes mixers 259 and 261, the outputs of which are applied to an adder-subtractor 263. An output of that adder-subtractor is applied to and accumulator/integrator 265.

20 The mixer 251 of the first correlator receives an early code replica 267 from a local code generator (not shown in Figure 7). Similarly, the mixer 253 receives a late code replica 269. The result is an output 271 of the accumulator having a form shown in
25 Figure 9A. The delay between the early and late replicas 267 and 269, respectively, is designated to be d . This is the same as specifying the early signal 267 to be $d/2$ ahead of the central reference phase 279 (Figure 9) and the late local code 269 being $d/2$ behind that reference t . It will be recognized that the output
30 271 shown in Figure 9A is similar in shape to that of Figure 6C.

Rather than relying simply on that correlator output, however, the second correlator receives in lines
35 273 and 275 a locally generated code having a difference between the early and late locally generated codes that

is 2d apart. An output 277 of the accumulator 265 is illustrated in Figure 9B. It will be noted that the curve of Figure 9B also generally has the same shape as that of Figure 6C but is different than that of Figure 9A in having a longer slope central portion. This also results in the magnitude in the flat portions of the curve being higher than that of the curve of Figure 9A.

It is in the combination of these two outputs in another adder-subtractor 283 that an error signal 285 of the form illustrated in Figure 9D is obtained. This characteristic is very advantageous since it contains extended portions 287 and 289 where the error signal is zero. This is accomplished, prior to combining the accumulator outputs 271 and 277 in the mixer 283, by reducing the magnitude of the accumulator output 277 by one half with an element 278, resulting in the curve of Figure 9C. This attenuation level is mathematically related to the difference in the widths of the two early-late correlators. The curve of Figure 9C is, in effect, subtracted from that of Figure 9A in the adder-subtractor 283, which gives the desirable error signal characteristic curve of Figure 9D. An operating range 281 exists around the in-phase point 279 wherein the circuit of Figure 7 adjusts the local code generator to drive the error signal of Figure 9D to zero at the in-phase point 279. However, any signal having a relative phase in either of the regions 287 or 289 will not affect the locking of the loop. As shown in Figure 9D, the local code generator can be locked exactly on the line-of-sight signal 213 without any contribution by the multipath signal 215. This occurs so long as the phase delay τ between the vectors 213 and 215, in a fraction of a chip, is greater than that of the operating range 281. Thus, under that circumstance, the effect of the multipath signal on the DLL correlator is completely eliminated.

Because of the wide extent of the zero error signal regions 287 and 289, it can be difficult to initially acquire a signal. That is, when the receiver is first powered up, if the relative phase of the local code generator causes the line-of-sight signal 213 to fall within one of the regions 287 and 289, there will be no error signal to adjust the phase of the local codes being generated. Therefore, a switch 291 (Figure 7) is provided to disconnect the second correlator from the circuit during initial signal acquisition. Thus, during such acquisition, the correlator characteristic output of Figure 9B is non-existent but rather that of Figure 9A. Thus, the multipath signal has some influence during this initial signal acquisition period but it is the purpose of the technique to bring the line-of-sight signal 213 within the operating range 281. Once this occurs, the switch 291 is closed. This then eliminates the influence of the multipath signal. The DLL correlator brings the line-of-sight signal 213 exactly in coincidence with the in phase position 279.

Quantitatively, a $d=0.1$ chip has been found satisfactory. This means that the operating range 281 is 0.1 chip, a very narrow region. In this example, the early - late of the second correlator whose output is illustrated in Figure 9B is twice that of a first correlator whose output is shown in Figure 9A. This results in each of the zero error signal regions 287 and 289 being 0.8 chip in duration, 80% of a possible relative phase difference is between the locally generated code and the PRN code that is part of the signal being received.

There are many variations in the specific parameters that can be selected for operation of the correlator of Figures 7 and 9. The specific early-late phase differences that are chosen for the two correlators may be within a wide range, so long as they

are different, depending upon a particular application and what is desired to be achieved. It is generally preferable, however, that one of the two correlators of Figure 7 have an early PRN code that is one $1/2K$ earlier than the in-phase locked position t , and its late PRN code $1/2K$ after t . Similarly, the second correlator has an early PRN code $N/2K$ ahead of t , and a late PRN code $N/2K$ after t . N and K are integers with N being smaller than K . In the example being described, $N=2$ and $K=10$. If these constraints are followed, the scaling factor of the element 278 of Figure 7 remains at $1/2$. If some other relationship between the two correlators is maintained, that scaling factor will generally need to be something different so that extended zero error signal regions 287 and 289 result when the accumulator output of Figure 9C is subtracted from that of Figure 9A.

Figure 8 shows a modification of Figure 7 wherein four accumulators are used, instead of the two accumulators 257 and 265 of Figure 7. The purpose of Figure 8 is to show that the same result is obtained if the outputs of each of the individual mixers 251, 253, 259 and 261 are accumulated prior to any combination of any of those outputs. An adder-subtractor 293 then receives outputs of the four accumulators, two of which now need to be scaled and switched rather than the single output 277 of Figure 7.

An alternative to the use of early-late correlators, but which gives the same beneficial results, is illustrated in Figure 10. A received signal 301, as previously described with respect to Figures 4, 7 and 8, is applied to a mixer 303 which also receives a replica 305 of the carrier contained in the signal 301. A signal 307, having a local carrier removed, is mixed in a mixer 339 with a gating sequence 341 from a local gating signal generator 343. The mixed signal

output of the mixer 339 is applied to an accumulator/integrator 345 whose output 347 is the error signal that is used to adjust the phase of the output of the local gating signal generator 343 to minimize the error signal.

Operation of the DLL correlator of Figure 10 can be illustrated by reference to the curves of Figure 11. Figure 11A illustrates PRN code that is modulated onto a carrier as part of the received signal 301. The code is a binary one, either being a plus one in level or a negative one in level. One of these levels is chosen to represent a binary bit one, and the other a binary bit zero. Transitions between these levels occur at one chip intervals. The code does not transition between levels every chip, however, but rather its information is contained in the pseudo-random manner in which it stays for one or more chips at one value and then switches to another value for one or more chips, and then back again, and so on.

Figure 11B shows one gating sequence 341 that may be utilized, it having a positive one value at each positive going transition of the incoming code of Figure 11A, and a negative one value at each negative going transition of the incoming code. The gating sequence 341 is zero (Figure 11B) when there is no transition where such a transition is possible. The transition of the gating sequence of Figure 11B coincides with a middle of each chip of the incoming code. The result of using the gating sequence of Figure 11B is an error signal 347 which has essentially the same function as that shown in Figure 5D. That is, the DLL correlator of Figure 10, when its gating sequence 341 is that of Figure 11B, provides essentially the same result as the DLL correlator of Figure 4 with its locally generated early-late PRN codes separated by one chip.

Figure 11C shows a gating sequence 341 which gives an error signal 347 that is essentially the same as that shown in Figure 6C. Coincident with each transition of the incoming code 11A is a pulse having a duration of 0.1 chip. The polarity of the pulse is positive during a positive transition of the incoming code and negative during a negative transition of the incoming code. The width of the pulse can be something other than 0.1 chip, which will then give an error signal function that is something different than that shown in Figure 6C.

Figure 11D shows a local gating sequence according to one aspect of the present invention. Use of this form of the gating sequence 341 (Figure 10) gives an error signal 347 having essentially the same function as that shown in Figure 9D. In order to achieve this, the gating sequence includes, coincident with the occurrence of each transition of the incoming code of Figure 11A, a pulse that has both positive and negative values. The gating sequence 341 is a zero value in between these pulse functions. These pulse functions are considerably less than one chip in duration. Each pulse function has equal positive and negative areas. When phase lock is achieved, a central portion of the pulse function of Figure 11D is aligned with the transition of the incoming code of Figure 11A. If that transition is positive going, then the polarity of the central portion of the pulse function of Figure 11D is of one polarity, and if the incoming code transition is negative going, that pulse function central portion has an opposite polarity. In Figure 11D, it is shown that the central portion at a time 349 coincident with a positive going edge of the incoming code of Figure 11A is positive, and that the pulse function central portion at a time 351 coincident with

a negative going edge of the incoming code of Figure 11A is negative, but these may be reversed.

Referring to Figure 12, characteristics of the pulse functions of Figure 11D will be explained with respect to the expanded scale diagram. A single pulse function occurring about the incoming code transition 349 can be viewed as having four distinct adjacent components. A central portion of the pulse function have areas 353 and 355 that are equal in area to each other on opposite sides of the transition line 349 when the error signal of the correlator of Figure 10 is minimized. Areas 357 and 359 have an opposite polarity to areas 353 and 355 and occur, respectively, ahead of and behind the pulse function areas 353 and 355. The areas 353 and 357 are caused to equal each other. Similarly, the areas 355 and 359 are caused to equal each other. In the specific example being described, the areas 353 and 355 have a width of 0.1 chip with a plus 1 magnitude while each of the areas 357 and 359 has a width of one half that or 0.05 chip, with a minus one magnitude.

Referring to Figure 13, curves are given to illustrate the relative tracking error boundaries for various multipath signals having different values of delay from the line of sight signal desired to be locked onto. The outer-curves 361 and 363 show the results of operating the DLL correlator of Figure 4 in a manner described with respect to the curves of Figure 5. The dashed lines 365 and 367 illustrate operation of the DLL correlator of Figure 4 in accordance with the curves of Figure 6, as described previously. It can be seen that the tracking error is considerably reduced but still is significant. A curve 369 of Figure 13 shows how the error is considerably reduced when one of the DLL correlators of Figures 7 or 8, as explained with respect to the curves of Figure 9, is utilized. The same

result, illustrated by the curve 369, occurs by using the gating sequence of Figure 11D with the correlator of Figure 10, as previously described. It will be noted from the curve 369 that multipath signals which are
5 delayed from the line of sight signal by any significant amount do not affect the tracking at all.

More specifically, Figure 13 shows in nanoseconds (ns) the envelope of zero tracking error for the three DLL correlators ϵ versus the delay τ in ns,
10 for a ratio α of the magnitude of the multipath signal to that of the line-of-sight signal is 0.5 with θ varying between $-\pi$ and $+\pi$. It is obvious that for τ between 0 and 10ns, the zero tracking error is roughly identical for the three correlators, and for τ around
15 100ns the advantage is clearly in favor of the 0.1 chip edge DLL. After 150ns, the zero tracking error becomes negligible for the $d=0.1$ chip edge correlator, whereas it stays at 30ns in the narrow correlator and above and increasing for the 1 chip wide correlator.
20 Conceptually, the edge DLL correlator used on C/A code is equivalent to a DLL correlator used on P code, and has the same beneficial multipath mitigation properties.

Embodiment of a GPS Receiver

The following description is mainly oriented
25 towards the United States' Global Positioning System (GPS); however it can also be applied to the Common Independent States' GLOBAL NAVIGATION Satellite System (GLONASS) as well, or to any ranging system using a PRN sequence. This embodiment is described with one bit
30 quantization; this choice, made for the sake of the simplicity of the description, does not preclude any constraint on the quantization.

Referring to Figure 14, a general block diagram of a pseudo-random noise (PRN) receiver 10 that
35 implements the present invention. The receiver 10

includes an antenna 11, a downconverter 12, multiple channels 13a to 13n, an input/output interface 14, and a digital processor 15. The antenna 11 receives a composite signal RF, composed of signals from all satellites in the system that are directly in the line of sight of the antenna. The composite signal RF is fed to the down-converter 12 to provide a quantized and sampled intermediate frequency signal IFW, a system sampling clock F_t and a SYSTEM CLOCK.

The signal IFW is a word of 4 bits, each representing one of four IF consecutive samples at a F_s sampling rate. The processing clock F_t is a division by 4 of the F_s signal. The system clock is a further division of F_t signal, interrupting the processor at a rate of approximately 1 per millisecond and triggering the channel processing.

Referring to Figure 15, the down-converter is discussed. The RF signal is first prefiltered by the RF filter 120, amplified by 121, and mixed with the Local Oscillator (LO) by the mixer 122, filtered and amplified again in IF by 123 and 124, and finally quantized in one bit by the hard limiter 125. The filter 123 is in fact used as a pre-correlation filter with a two-sided bandwidth of 20.46Mhz. The instantaneous hard limiter output is sampled at a rate of F_s , and shifted in the 4-stage shift register 126. The sampling rate F_s is chosen to satisfy the Nyquist rate requirement, related to the pre-correlation filter bandwidth. Every F_t clock transition (i.e. 4 F_s clocks), the full contents of the shift register is transferred into a parallel register 127. The 4 bit word IFW is then transferred to the channel circuits at a F_t rate for satellite individual tracking.

The clock reference circuitry of the down converter (Figure 15) includes a phase lock loop (PLL) which is composed itself of the voltage controlled

oscillator (VCO) 131, a frequency divider 132, a phase comparator 129, which compares the phase with a stable reference oscillator 128, and, finally, a low frequency loop filter 130. The VCO output is used as local oscillator for the RF section. The frequency of the VCO 131 is divided in several steps, a first time by a divider 133 to get the sampling frequency F_s , a second time by a divider 134 to get the processing clock F_t , and a third time by a divider 135 to get the SYSTEM CLOCK.

As shown in Figure 14, the sampled and quantized intermediate frequency signal IFW is simultaneously fed to each of the several signal processing channels 13a to 13n. A separate channel 13 is devoted to every visible satellite; the assignment to a given satellite is made by configuring the pseudo-random noise (PRN) generator through the PRN GENERATOR COMMANDS. The structure of a channel 13, typical of each of the channels 13a-13n, is given in Figure 16. Every satellite signal is simultaneously tracked in carrier phase by a carrier Phase Lock Loop (PLL) and in code phase by a Delay Lock Loop (DLL). All channel processing is made in a fully synchronous manner at a processing clock F_t . IFW samples are processed 4 by 4, and all carrier and code generation is made at F_t rate by groups of 4 as well.

Both the PLL and the DLL are implemented partly in the channel 13, and partly in the processor 15. The link is made by the I/O interface 14. The loop comparators and the loop actuators are located in each channel, whereas the filter implementation and the loop management are handled by the processor 15. The loops are updated when the processor is interrupted by the SYSTEM CLOCK signal and the MEAS READY signal is set for that channel, informing the processor that a measurement cycle has just finished. All measurement cycles are

chosen at a period bigger than that of the SYSTEM CLOCK, in order not to miss any measurement. The cycle period is set by the processor at every channel initialization, through the PRN GENERATOR COMMAND.

5 The carrier PLL uses the measurements I and Q of an in-phase correlator 130a, and a quadrature phase correlator 130b. In a tracking mode, the PLL drives the information Q to zero while checking for the presence of the signal locking on I. Both correlators are using the
10 same "punctual" pseudo-random code (PRN) for the correlation, but use different carrier signals COS and SIN. The processed information is used to control the CARRIER FREQUENCY COMMAND of a carrier numerically controlled oscillator (NCO) 132.

15 The carrier NCO 132 is described in detail in Figure 17. The instantaneous carrier phase image is kept in a carrier phase register 1325, where the total range represents 2π of carrier phase. The current CARRIER FREQUENCY COMMAND is kept in a frequency command
20 register 1323. At every Ft transition, this value is added to the current carrier phase register contents by the adder 1321c; thus, the carrier phase is incremented one full cycle every time the carrier phase register 1325 cycles back to zero.

25 The instantaneous carrier phase can be obtained at any SYSTEM CLOCK transition or at every Ft very straightforwardly; the carrier phase register 1325 is reset synchronously with the SYSTEM CLOCK at the initial CHANNEL RESET command, ensuring a known initial
30 phase. Every processor command loaded into a buffer 1324 is transferred into the frequency command register 1323 and effective at the next SYSTEM CLOCK transition; as the SYSTEM CLOCK period is an exact number of Ft periods and knowing the loaded command word, the exact
35 value in the carrier phase register is obtained at the

next SYSTEM CLOCK transition or at any F_t clock transition in between by direct computation.

5 The one bit reference carrier cosine value C_0 is obtained by "exclusively ORing" the most significant bit (MSB) and the second most significant bit of the carrier phase register contents. The one bit reference carrier sine value is obtained using the MSB of carrier phase register contents; this is actually done in the phase/quadrature signal generator 1320c.

10 As the samples are processed 4 by 4, the carrier references are generated synchronously with the exact sampling times for the 3 other samples as well. Arbitrarily and for simplicity of implementation, the reference signal is chosen to be the third of the sequence of 4.

15 If may be noted that the carrier phase 1325 is physically incremented by the frequency command value 1323 every F_t . It is equivalent to say that the instantaneous carrier phase is virtually incremented by a fourth of this value every F_s (i.e. four times per F_t period). As a result, the reference carrier phase synchronous with the fourth sample (most recent one) is obtained by adding frequency command divided by four (divider 1322c) to the current carrier phase 1325; the carrier cosine (sine) value C_{+1} (S_{+1}), delayed of one sampling period, is obtained from it with the phase quadrature signal Generator 1320d using the same algorithm as for C_0 and S_0 .

25 Similarly, C_{-1} , S_{-1} are obtained by subtracting frequency command value divided by 2 using 1322a from the current carrier phase 1325. This subtraction is performed by using the adder 1321a. The cosine and sine values are finally obtained through 1320a.

30 Finally C_{+2} , S_{+2} are obtained by subtracting the frequency command value divided by 4 using 1322b from the current carrier phase 1325. This subtraction is

made using the adder 1321b. The cosine and sine values are finally obtained through 1320b.

The full NCO output is a "cosine" word COS and a "sine" word SIN of 4 bits each, each bit being the sampled carrier reference value one sample apart. The "punctual" in-phase (130a) and quadrature-phase (130b) correlators for the PLL are described in Figure 19. Given the close similarity, the following correlator description deals with only the in-phase case.

The intermediate frequency word IFW composed of 4 samples is "exclusive ORed" with the 4 bit cosine carrier reference COS in the structure 1301a to 1301d. All samples are added in the adder 1302; the result is comprised between -4 and +4 (the "0" values are processed as "-1" by the adder 1302). The result is then multiplied by the value of reference PRN sequence synchronous with the most recent sample (multiplier 1303). The resulting value is then algebraically added at a Ft rate to the current contents of the accumulator 1305. At every CYCLE transition the accumulator value is transferred to the buffer, the accumulator is reset, and finally a new measurement period is initiated. The processor is then able to read the measurement values to close the loops.

Going briefly back to Figure 16, the delay lock loop will be described in more detail. The DLL has 2 configurations, acquisition mode or tracking mode, depending on the channel locking phase. As described in the prior section, the tracking mode preferably uses an "edge DLL" correlator, while the acquisition mode uses a 0.1 chip delay DLL. The selection between 2 modes is made through the signal DLL SELECT. Other specific combinations of tracking and acquisition mode correlators may also be employed.

The delay lock loop (DLL) processing is timed at a Ft rate similarly to the PLL, and the measurement

update rate is CYCLE as well. The DLL uses dI and dQ information coming from an in-phase DLL correlator 131a for dI, and a quadrature phase DLL correlator 131b for dQ. The DLL drives the dQ value to zero when in tracking mode. The dQ is used in conjunction with dI when in acquisition mode. The processed information is used to control the PRN GENERATOR COMMANDS of the PRN Code Generator 133.

The "edge DLL" principle, previously described with respect to Figures 10, 11D and 12, will be described in more detail, in light of the GPS receiver just described. For "edge DLL" implementation purposes, four time intervals of equal duration have to be defined around the PRN code transition; two before the code transition and two after. In the current embodiment, each time interval has an exact duration of $1/F_s$ or the IF sampling period.

We thus infer that every time interval contains one and only one IF sample at a F_s rate. The relative position of the samples in the interval is unknown and depends on the relative phase between code generator and sampling clock. The full formula expressing the DLL response is given below.

Assume that $S_{-2}, S_{-1}, S_{+1}, S_{+2}$ is a sequence of four consecutive IF samples with the code transition between S_{-1} and S_{+1} , and the associated sampled PRN code

sequence is $PRN_{-2}, PRN_{-1}, PRN_{+1}, PRN_{+2}$ (with $PRN_{-2} = PRN_{-1}$ and $PRN_{+1} = PRN_{+2}$). $dPRN$ may be defined as:

$$dPRN = \frac{1}{2} \cdot (PRN_{+1} - PRN_{-1})$$

Thus $dPRN$ equals:

- +1, if the transition is a rising edge,
- 1, if the transition is a falling edge,
- 0, if two consecutive PRN chips are identical.

$dPRN$ can be thought as the derivative of the PRN sequence.

At every PRN chip code transition, the elementary DLL contribution is given by:

$$DLL_i = (-S_{-2} + S_{-1} + S_{+1} - S_{+2}) \otimes dPRN$$

The contribution is not zero if $dPRN \neq 0$ (i.e. if $PRN_{-1} \neq PRN_{+1}$).

After an integration period defined between two contiguous CYCLE transitions, the full DLL response will be:

$$DLL = \sum_i DLL_i$$

This summation performs a low pass frequency filtering function of the measurements dI and dQ .

Going back to the physical implementation, we notice that knowing a code transition falls inside a

group of 4 IFW samples, we still have to know between which samples of the group the code transition falls. The signals P0 and P1 show where the code transition falls among the 4 IFW samples. Because we need to add 4 consecutive values and the code transition can have 4 different positions in the sequence, we need to keep the 3 previous samples of the previous sequence of 4 IFW. The total sequence will be, from the oldest sample to the newest: S_{2A} , S_{3A} , S_{4A} , S_1 , S_2 , S_3 , S_4 and PRN₄, being the PRN code synchronous with S_4 .

P1 value	P0 value	code transition falls between	Elementary DLL operation in tracking mode	Elementary DLL operation in acquisition mode
0	0	S_{3A} and S_{4A}	$(-S_{2A} + S_{3A} + S_{4A} - S_1) \odot \text{PRN}$	$(+S_{2A} + S_{3A} + S_{4A} + S_1) \odot \text{PRN}$
15 0	1	S_{4A} and S_1	$(-S_{3A} + S_{4A} + S_1 - S_2) \odot \text{PRN}$	$(+S_{3A} + S_{4A} + S_1 + S_2) \odot \text{PRN}$
1	0	S_1 and S_2	$(-S_{4A} + S_1 + S_2 - S_3) \odot \text{PRN}$	$(+S_{4A} + S_1 + S_2 + S_3) \odot \text{PRN}$
1	1	S_2 and S_3	$(-S_1 + S_2 + S_3 - S_4) \odot \text{PRN}$	$(S_1 + S_2 + S_3 + S_4) \odot \text{PRN}$

Table 1

20

Going to Figure 20, the implementation of the In-Phase DLL correlator 131a is described in detail. After multiplying IFW by the Carrier word COS by 1310a to 1310d, the three last samples of the current IFW word are latched in 1318. At the input of the four multiplexors 1311a to 1311d, seven samples are simultaneous available, S_1 to S_4 from the current IFW and S_{2A} to S_{4A} from the preceding one. Depending on the current value of P1 and P0, a common selection is made on all 4 multiplexors. For the remaining of the explanation, we will assume that $P0=P1=0$. On 1311a output, S_1 is available; on 1311b, S_{4A} is available, and so on. The adder 1313 adds up all selected samples (interpreting "0" inputs as "-1" value in the process). The result is then multiplied by dPRN to form the elementary value DLL_1 . In tracking mode, the signal DLL

35

SELECT will invert the values coming out from the first and the last multiplexor, thus fully implementing the tracking DLL formula described in the first line of the Table 1.

5 The current value between +4 and -4 is algebraically added to the accumulator 1316 by the adder 1315 during the same Ft transition. Every transition on CYCLE transfers the accumulator value to the buffer 1317, resets the accumulator, and finally initiates a
10 new measurement period.

 There is only a slight difference when implementing the acquisition mode. The circuitry is identical up to the adder 1313, except that the first and last sample coming out from the multiplexor 1311a
15 and 1311d are not inverted. The dPRN signal is defined the same way than previously, but its size is expanded to reach 0.1 code chip duration, centered on the code transition.

 Referring to Figure 18, the full PRN code
20 generator will be described. The Generator is in fact composed of a code numerically controlled oscillator (NCO), which delivers a chip frequency clock Fc whose frequency is in direct control of the processor through the CODE FREQUENCY COMMAND; in turn, Fc clocks the PRN
25 code generator 1334 per se.

 Let's begin by the Code NCO description: similarly to the carrier NCO, it is embodied by a code phase register 1335, whose full range represents 2π of the code phase. At every Ft transition, the word into
30 code frequency command register 1336 is added (modulo the range of code phase register) to the contents of the code phase register by the adder 1331d. The carry signal coming from the adder is used as chip frequency Fc. The CODE FREQUENCY COMMAND word present in the code
35 frequency command register is loaded at every SYSTEM CLOCK transition from the buffer 1337. The buffer is

itself loaded from the processor at any time. Another important function of the code NCO is to deliver the signals P0 and P1, whose function was described earlier.

The P0 and P1 signals are generated as follows: if R is the total range of the code phase register (CPR) 1335, and $\Delta\phi$ is the phase increment at every F_s sample ($\Delta\phi = \text{CODE FREQUENCY COMMAND} / 4$).

	$0 < \text{CPR} \leq \Delta\phi$	$\Delta\phi < \text{CPR} \leq 2\Delta\phi$	$2\Delta\phi < \text{CPR} \leq R - 2\Delta\phi$	$R - 2\Delta\phi < \text{CPR} \leq R - \Delta\phi$	$R - \Delta\phi < \text{CPR} \leq R$
P1	0	0	1	1	1
P0	1	0	0	1	0

Table 2

P1 is obtained by subtracting the Code Frequency Register (CFR) 1336 divided by two (by divider 1332b) from the Code Phase Register (CPR) 1335 by use of the adder 1331c. If the result RES1 is positive, P1 = 1.

The P0 case is different depending on the P1 value. If P1 is zero ($\text{CPR} < 2\Delta\phi$), CFR, divided by four (by divider 1332a), is multiplied by -1 in the multiplier 1331b; if P1 is one ($\text{CPR} \geq 2\Delta\phi$), CFR/4 is multiplied by +1. Then 1331a adds RES1 to the multiplication result; the carry of the adder 1331a is taken as P0. The final result is in agreement with Table 2.

The PRN code generator 1334 is clocked by the chip frequency F_c . It is configured for a particular satellite sequence by the command GENERATOR PRESET. It outputs an epoch signal, synchronous with a particular instant in the PRN sequence, which is taken as reference in the PRN ranging sequence. The data bits superimposed on the PRN sequence have their transition perfectly synchronous with this epoch signal.

The EPOCH signal clocks the cycle counter 1333, which is reset at the initialization of the channel by the SYNC RESET, and counts an integer number of epochs (preset at the preset sequence) before to
5 generate a transition on CYCLE, which stops the current measurement cycle on all correlators and informs the processor by the signal MEAS READY. Every channel has its own cycle counter, synchronized on its own data transitions. After a synchronizing phase on the data
10 transitions, it is possible to slow down the measurement periods up to 20ms, no data transitions occurring during this period.

It is assumed, accurately, that the edge DLL correlator used on C/A code, with a precorrelation
15 bandwidth prefiltering (typically 20.46Mhz double sided) improves the multipath error. A PRN code transition detector is built X-ORing the current code output and the previous one latched in the latch 1339. The signal dPRN is generated by 1338 according to the
20 description in the DLL principle explanation.

According to the usual multipath model, the direct received signal is given by:

$$A \cdot PRN(t) \cdot \cos(\omega_0 t + \varphi)$$

where:

A is the amplitude of the received signal

25 PRN(t) is the pseudo-random sequence

ω_0 is the carrier frequency pulsation

φ is the carrier phase offset

The multipath signal is given by:

$$A \cdot \alpha \cdot PRN(t - \tau) \cdot \cos(\omega_0(t - \tau) + \phi - \theta)$$

where:

α is the amplitude ratio between direct and multipath signal

5 τ is the propagation delay between direct and multipath signal

θ is the additional phase rotation between direct and multipath signal.

10 The main effect of the presence of a multipath signal is to shift the zero crossing of the DLL response from the "zero multipath" reference differently for each of the three discriminators. The DLL driving the DLL correlator output to zero in average, the difference between zero crossings will be seen directly as an error
15 in the measured code phase. As the different satellites on which the channels do not experience the same multipaths because of a different geometry, the position computation will be erroneous.

20 Returning to the above description, with respect to Figures 11D and 12, of operation of a receiver that uses the demodulation technique of Figure 10, a few alternate local gating sequences will be described. Figures 21B, 21C and 21D give other examples
25 of what the gating signal generator 343 can provide in line 341. The result in terms of the error signal characteristic of Figure 9D is substantially the same, but the different gating sequences of Figures 21B-D cause the height and duration of the non-zero portions of the Figure 9D curve to change somewhat. The
30 fundamental advantage is retained, however, of providing extended intervals where the error signal is zero.

In each of Figures 21B-D, a carefully controlled gating signal occurs at each of transitions 365, 367, etc., of the incoming code (Figure 21A). In Figure 21B, negative portions 369 and 371 of the signal have a magnitude less than 1, while corresponding positive portions 373 and 375 have a magnitude of 1. The lower magnitude negative portions of the signal are given longer durations, however, so that the areas of the pulse portions 369 and 373 are equal, as are the areas 371 and 375. In the gating signal of Figure 21C, a positive area 377 (magnitude less than 1) is much smaller than a negative area 379 (magnitude more than 1), while a positive area 381 is much smaller than a negative going area 383. This gating signal differs from the others shown herein by aligning with the code signal edge 365 (when a minimum error condition exists) a transition between negative and positive going portions of the signal. Each of the signals of Figures 11D, 12, 21B and 21C is symmetrical about the code edge. The signals are positioned with their middle aligned with the code edge.

In Figure 21D, however, the gating signal is non-symmetrical about the incoming code edge. But the positive and negative going pulse portions have equal areas on each side of the code edge. That is, areas 385 and 387, on one side of the code edge 365, are substantially equal, while the areas 389 and 391 on the other side of the code edge 365 are also substantially equal.

Although several specific examples of compound gating pulse shapes have been given, there are numerous other shapes, with various relative magnitudes, that can be employed instead. The total negative and positive going areas of any such compound gating pulse is made to be substantially equal. This property causes the multipath signal to be substantially eliminated so long

as its delay from the line of sight signal is sufficient.

Although the various aspects of the present invention have been described with respect to their
5 preferred implementations, it is understood that the invention is protected within the full scope of the appended claims.

IT IS CLAIMED:

1. A method of decoding an incoming signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, comprising:

5 locally generating a PRN signal corresponding to the PRN code of the incoming signal,

mixing the locally generated PRN signal with the incoming signal,

10 developing, from a result of mixing the locally generated PRN signal with the incoming signal, an error signal having a magnitude as a function of a relative phase difference between the incoming signal PRN code and the locally generated PRN signal that (a) is zero for a zero relative phase difference and for a majority of a range of the relative phase difference between plus and minus one chip, and (b) increases as the relative phase difference changes from zero to another value within a central portion of said range, and

15 when the error signal has a non-zero magnitude within said central portion of said range, adjusting said relative phase difference by adjusting the phase of the locally generated PRN signal a manner to drive the error signal to zero, thereby to drive the relative phase difference between the incoming signal PRN code and the locally generated PRN signal to zero.

20 2. The method of claim 1 wherein the local generation of the PRN signal corresponding to the PRN code of the incoming signal includes generating an operating set of recurring non-zero gating signals representing edges of the PRN code and which

5 individually (a) are less than one chip in duration, (b) have equal positive and negative areas, and (c) have a positive or negative polarity at a center thereof

corresponding to whether a PRN code edge is positive or
10 negative going.

3. The method according to claim 2 wherein,
prior to locally generating said operating set of gating
signals, an initial set of non-zero recurring gating
signals are generated with recurring non-zero gating
5 signals that individually (i) are less than one chip in
duration, and (ii) have a single positive or negative
polarity that designates whether a PRN code edge is
respectively positive or negative going, thereby to
initially acquire an incoming signal before locally
10 generating the operating set of gating signals.

4. The method according to claim 1 wherein
the local generation of the PRN signal corresponding to
the PRN code of the incoming signal includes generating
as an operating set of PRN signals a first replica
5 advanced in phase $1/2K$ of said chip with respect to a
reference, a second replica delayed in phase $1/2K$ of
said chip with respect to said reference, a third
replica advanced in phase $N/2K$ of said chip with respect
to said reference, and a fourth replica delayed in phase
10 $N/2K$ of said chip with respect to said reference,
wherein N and K are integers with N being smaller than
 K .

5. The method according to claim 4 wherein
mixing of the incoming signal with the first, second,
third and fourth locally generated PRN code replicas
results in corresponding first, second, third and fourth
5 mixed signals, and wherein developing the error signal
includes giving the first and fourth mixed signals the
same polarity that is different from a common polarity
of the second and third signals.

6. The method of claim 4, wherein K equals 10 and N equals 2.

7. The method of claim 4 wherein, prior to locally generating the operating set of PRN signals, an initial set of PRN signals is generated that includes said first and second replicas without said third and fourth replicas, thereby to initially acquire an incoming signal before locally generating the operating set of gating signals.

8. The method of any one of claims 1-7 wherein the incoming signal includes at least a primary signal being received directly in a line of sight from a transmitter and a multipath version of the primary signal being received with a phase delay therebetween that is greater than said central portion of the error signal range, whereby the adjusting of the relative phase difference is performed with respect to the primary signal and not the multipath signal.

9. In a receiver of a radio frequency signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, a method of locking onto the PRN code of a primary signal received in a line of sight from a transmitter when a multipath version of that signal is also received with a time delay of a fraction of one chip, comprising:

generating a PRN signal corresponding to the PRN code of the received signal,

mixing the generated PRN signal with the received signal which includes both the primary signal and the delayed multipath version thereof,

adjusting a relative phase of the generated PRN signal in response to an error signal, and

15 initially generating the error signal from
comparing the phase of the generated PRN signal with the
phase of a composite of the primary and multipath
signals, and then subsequently generating the error
20 signal from comparing the phase of the generated PRN
signal with the phase of the primary signal without the
multipath signal.

10. The method of claim 9 wherein the
generation of the PRN signal includes generating an
operating set of recurring non-zero gating signals
representing edges of the PRN code and which initially
5 (i) are less than one chip in duration, and (ii) have a
single positive or negative polarity that designates
whether a PRN code edge is respectively positive or
negative going, and then subsequently (a) are less than
one chip in duration, (b) have equal positive and
10 negative areas, and (c) have a positive or negative
polarity at a center thereof corresponding to whether a
PRN code edge is positive or negative going.

11. The method according to claim 9 wherein
the generation of the PRN signal includes initially
generating a first replica advanced in phase $N/2K$ of
said chip with respect to a reference and a second
5 replica delayed in phase $N/2K$ of said chip with respect
to said reference, and then subsequently adding a third
replica advanced in phase $1/2K$ of said chip with respect
to said reference and a fourth replica delayed in phase
 $1/2K$ of said chip with respect to said reference,
10 wherein N and K are integers with N being smaller than
 K .

12. The method of claim 11, wherein K equals
10 and N equals 2.

13. A method of decoding an incoming signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, comprising:

5 locally generating recurring non-zero operating gating signals representing PRN code edges and which individually (a) are less than one chip in duration, (b) have equal positive and negative areas, and (c) have a positive or negative polarity at a center thereof that designates whether a PRN code edge is
10 positive or negative going,

mixing the incoming signal with each of the locally generated gating signals, thereby generating first and second mixed signals,

15 correlating and accumulating said first and second mixed signals, thereby obtaining a correlation signal, and

using the correlation signal to adjust the phase of the locally generated gating signals with respect to the PRN code of the incoming signal in order
20 to maximize the correlation, thereby to lock the phase of the locally generated gating signals to the phase of the PRN code in the incoming signal.

14. The method according to claim 13 wherein, prior to locally generating said operating gating signals, generating an initial gating signals with recurring non-zero gating signals that individually (i)
5 are less than one chip in duration, and (ii) have a single positive or negative polarity that designates whether a PRN code edge is positive or negative going.

15. The method according to claim 13 wherein the individual gating signals have a common duration in terms of a fraction of a chip of the PRN code of the incoming signal.

16. A method of decoding an incoming signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, comprising:

5 locally generating replicas of the incoming signal PRN code including a first replica advanced in phase $1/2K$ of said chip with respect to a reference, a second replica delayed in phase $1/2K$ of said chip with respect to said reference, a third replica advanced in phase $N/2K$ of said chip with respect to said reference,
10 and a fourth replica delayed in phase $N/2K$ of said chip with respect to said reference, wherein N and K are integers with N being smaller than K ,

mixing the incoming signal with the locally generated PRN code replicas,

15 combining and accumulating the mixed incoming and PRN code replicas, thereby obtaining a correlation signal, and

using the correlation signal to adjust the phase of the locally generated PRN code replicas with
20 respect to the PRN code of the incoming signal in order to maximize the correlation, thereby to lock the phase of the locally generated PRN code replicas to the phase of the PRN code in the incoming signal.

17. The method of claim 16, wherein K equals 10 and N equals 2.

18. The method of claim 16, wherein mixing the incoming signal with the first, second, third and fourth locally generated PRN code replicas results in corresponding first, second, third and fourth mixed
5 signals, and wherein combining and accumulating said mixed signals includes giving the first and fourth mixed signals the same polarity that is different from a common polarity of the second and third mixed signals.

19. The method of claim 18, wherein the combining and accumulating of said mixed signals is performed by first doing the accumulating and then doing the combining.

20. The method of claim 18, wherein the combining and accumulating of said mixed signals is performed by doing at least some of the combining before the accumulating.

21. A receiver of a composite radio frequency signal including a plurality of signals that individually include a carrier signal having encoded thereon a pseudo-random noise (PRN) binary code,
5 comprising:

means receiving the composite radio frequency signal for transforming the composite signal into an intermediate frequency signal, whereby the intermediate frequency signal includes a plurality of signals that
10 individually include an intermediate frequency carrier signal having the PRN code encoded thereon,

a plurality of channel circuits receiving the intermediate frequency signal, individual ones of said plurality of channel circuits including means for
15 decoding one of the plurality of intermediate frequency signals that comprises:

means responsive to an error signal for locally generating a PRN signal corresponding to the PRN code of the intermediate frequency signal with a relative phase controlled by a
20 magnitude of the error signal,

means for mixing the locally generated PRN signal with the intermediate frequency signal,

25 means using the mixed signal for generating an error signal having a magnitude

as a function of a relative phase difference between the PRN code of one of the intermediate frequency signals and the locally generated PRN signal that (a) is zero for a zero relative phase difference and for a majority of a range of the relative phase difference between plus and minus one chip, and (b) increases as the relative phase difference changes from zero to another value within a central portion of said range.

22. The receiver of claim 21 wherein the local PRN signal generating means includes means for generating an operating set of recurring non-zero gating signals representing edges of the PRN code and which individually (a) are less than one chip in duration, (b) have equal positive and negative areas, and (c) have a positive or negative polarity at a center thereof corresponding to whether a PRN code edge is positive or negative going.

23. The receiver of claim 22 wherein the local PRN signal generating means additionally includes means for generating an initial set of non-zero recurring gating signals that individually (i) are less than one chip in duration, and (ii) have a single positive or negative polarity that designates whether a PRN code edge is respectively positive or negative going, and wherein individual ones of the plurality of channel circuits includes means for selecting one of the operating or initial set of gating signals for mixing by the mixing means with the intermediate frequency signal.

24. The receiver of claim 21 wherein the local PRN signal generating means includes means for generating an operating set of PRN signals that includes

5 a first replica advanced in phase $1/2K$ of said chip with
respect to a reference and with a first polarity, a
second replica delayed in phase $1/2K$ of said chip with
respect to said reference and having a second polarity
opposite to the first polarity, a third replica advanced
10 in phase $N/2K$ of said chip with respect to said
reference and with said first polarity, and a forth
replica delayed in phase $N/2K$ of said chip with respect
to said reference and with said second polarity, wherein
N and K are integers with N being smaller than K.

25. The receiver of claim 24, wherein K
equals 10 and N equals 2.

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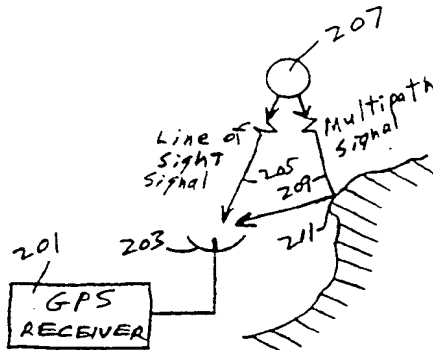


FIG. 1

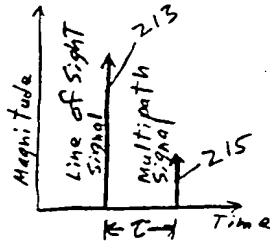


FIG. 2

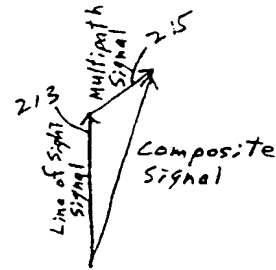


FIG. 3

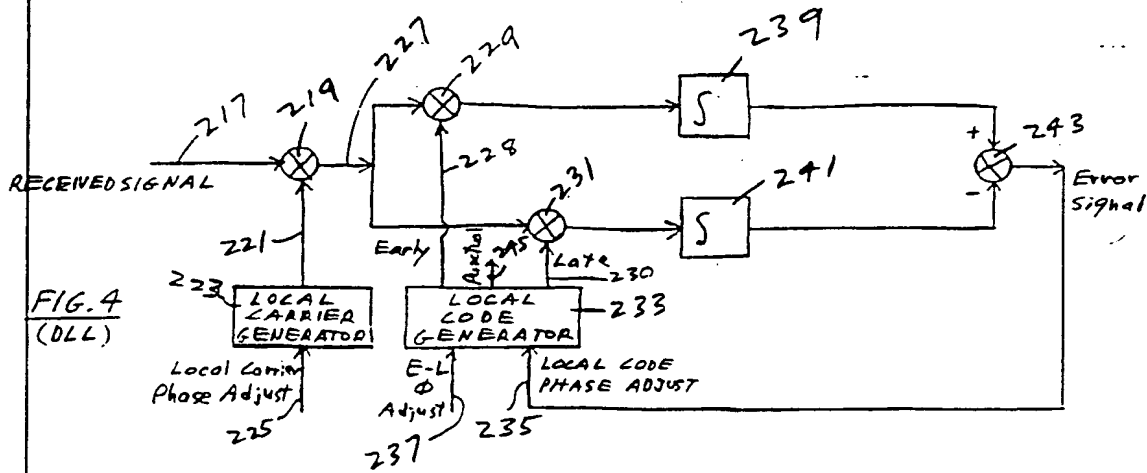


FIG. 4
(DLL)

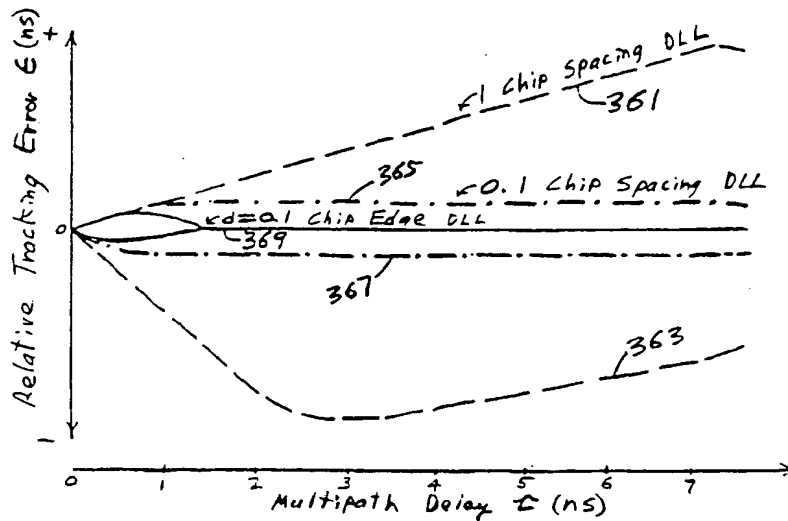


FIG. 13

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(2 of 13)

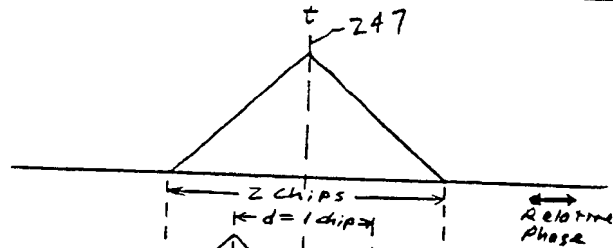


FIG. 5A
(Punctual)

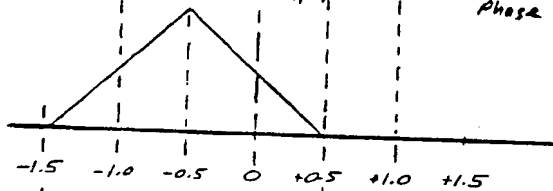


FIG. 5B
(Early)

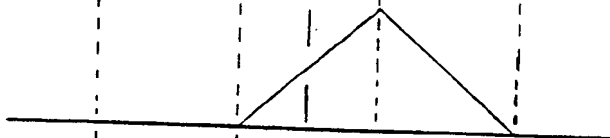


FIG. 5C
(Late)

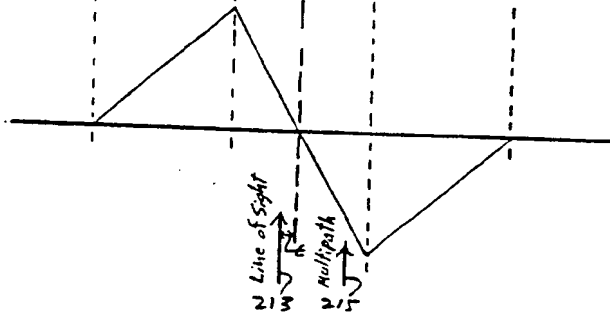


FIG. 5D
(Error Signal)

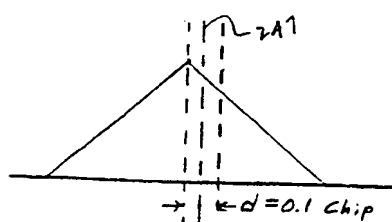


FIG. 6A
(Early)



FIG. 6B
(Late)

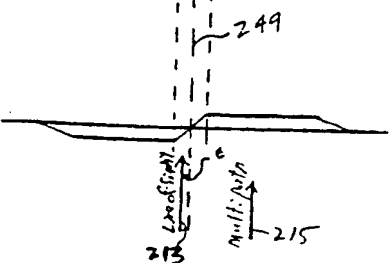
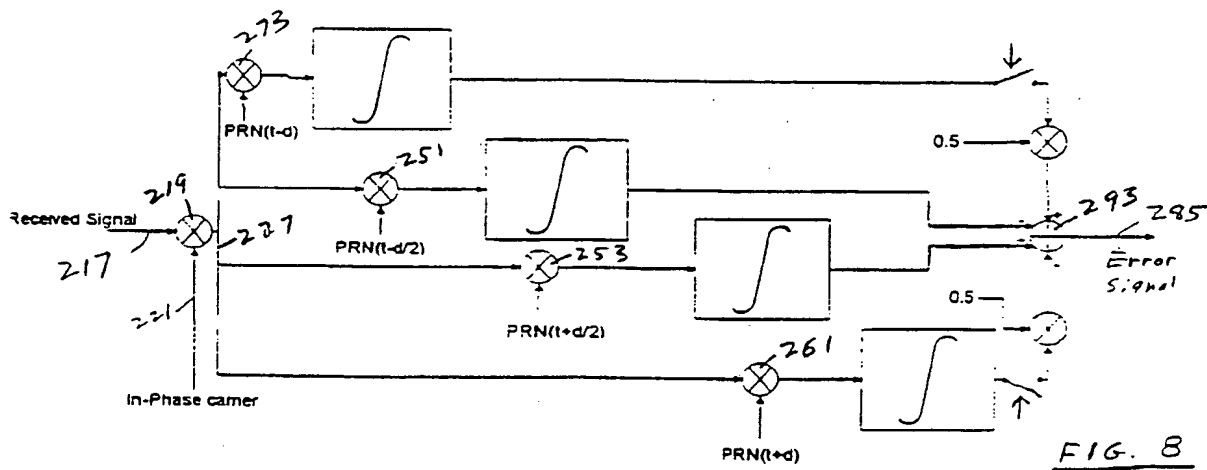
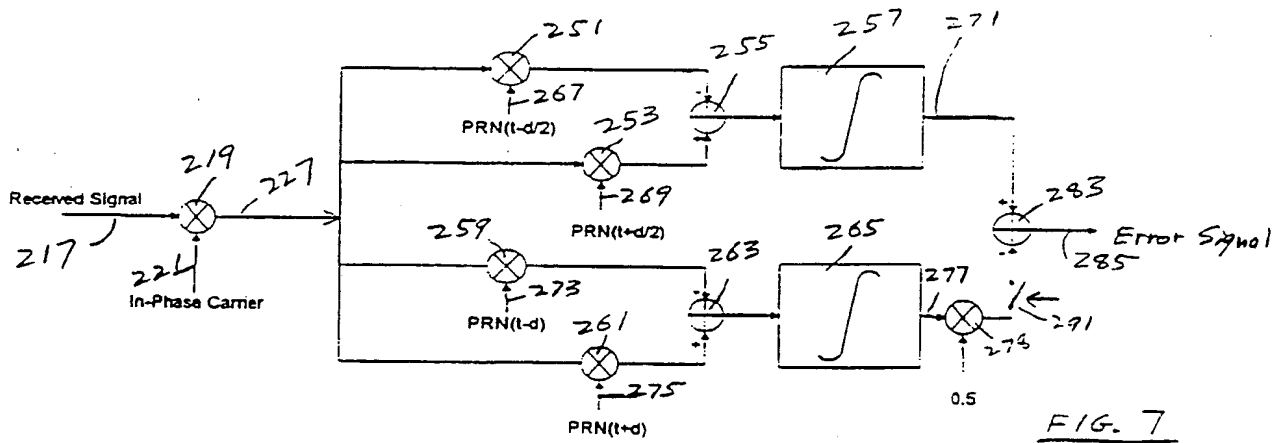


FIG. 6C
(Error Signal)

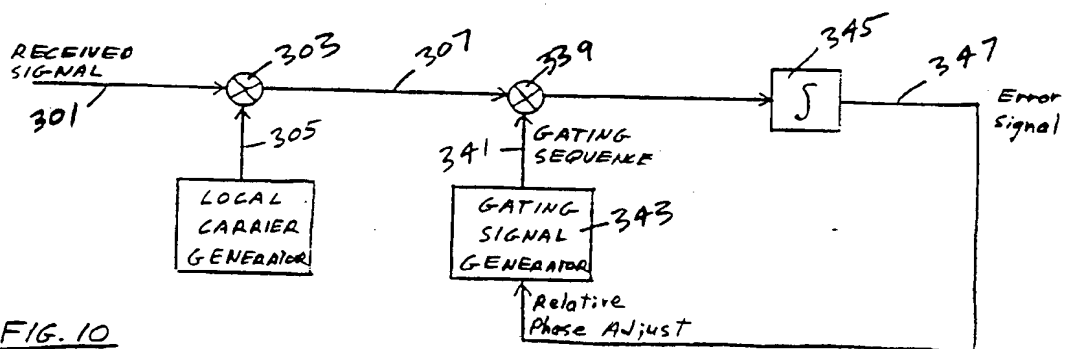
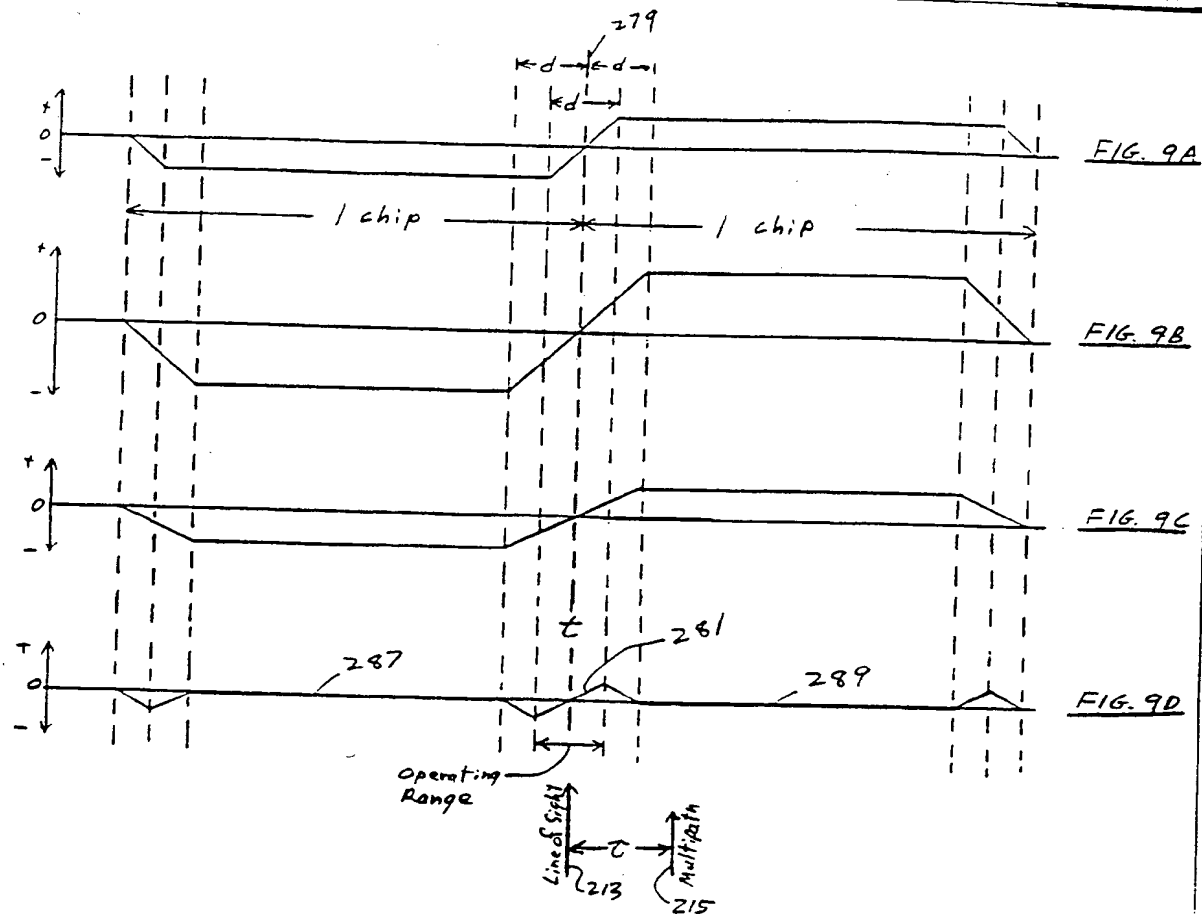
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FIG. 7-1100



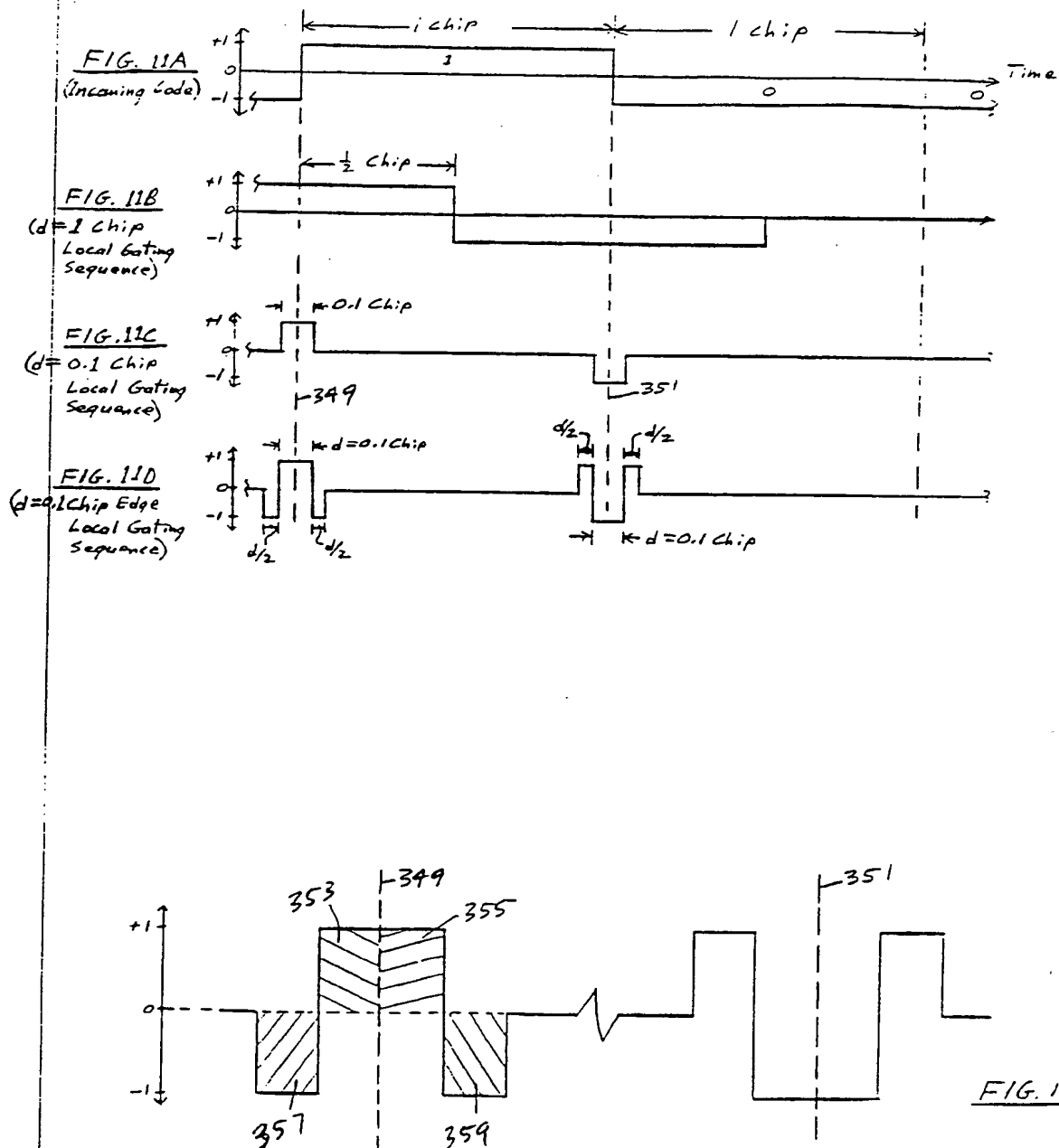
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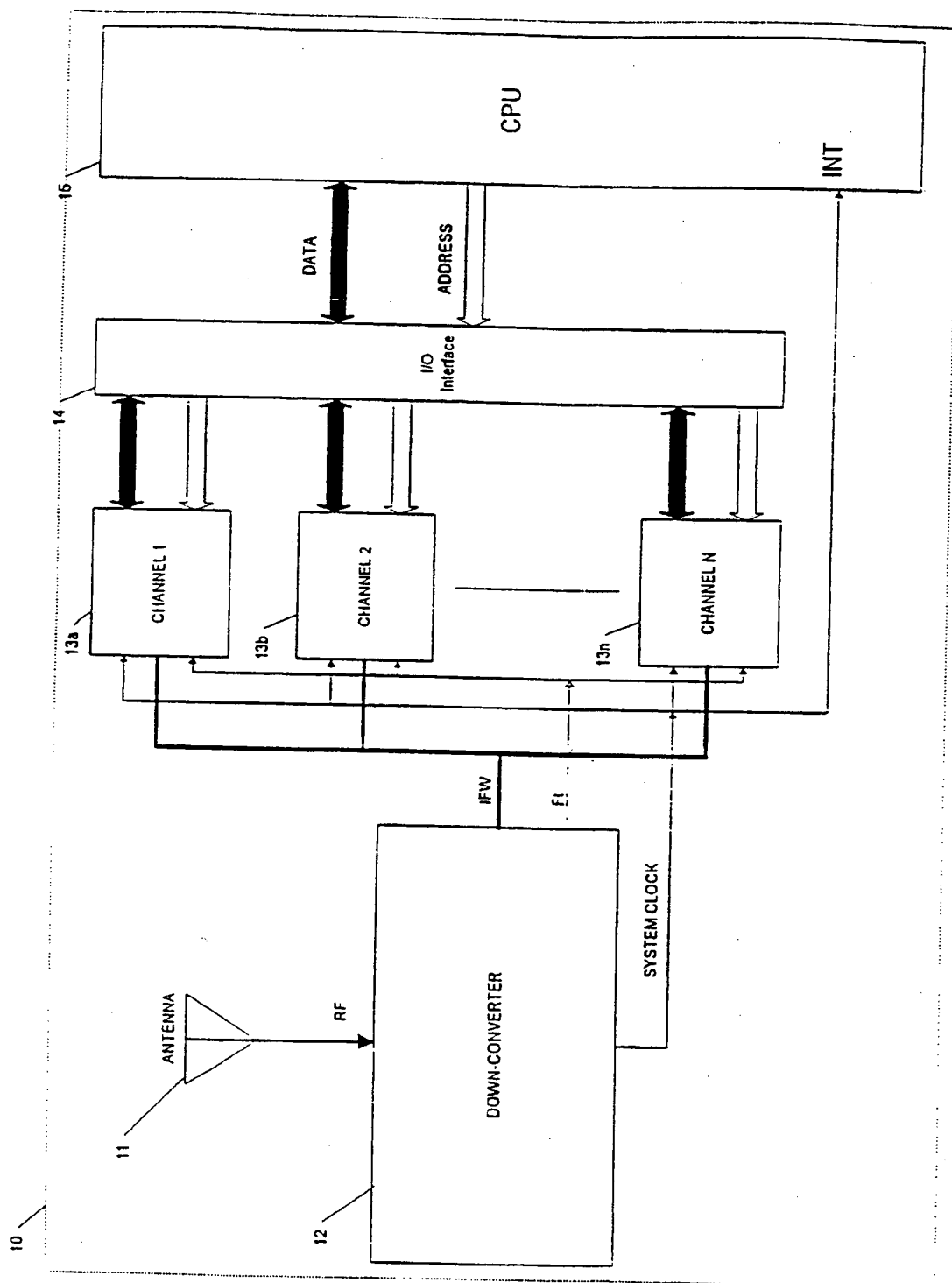


FIG 14
(Receiver System)

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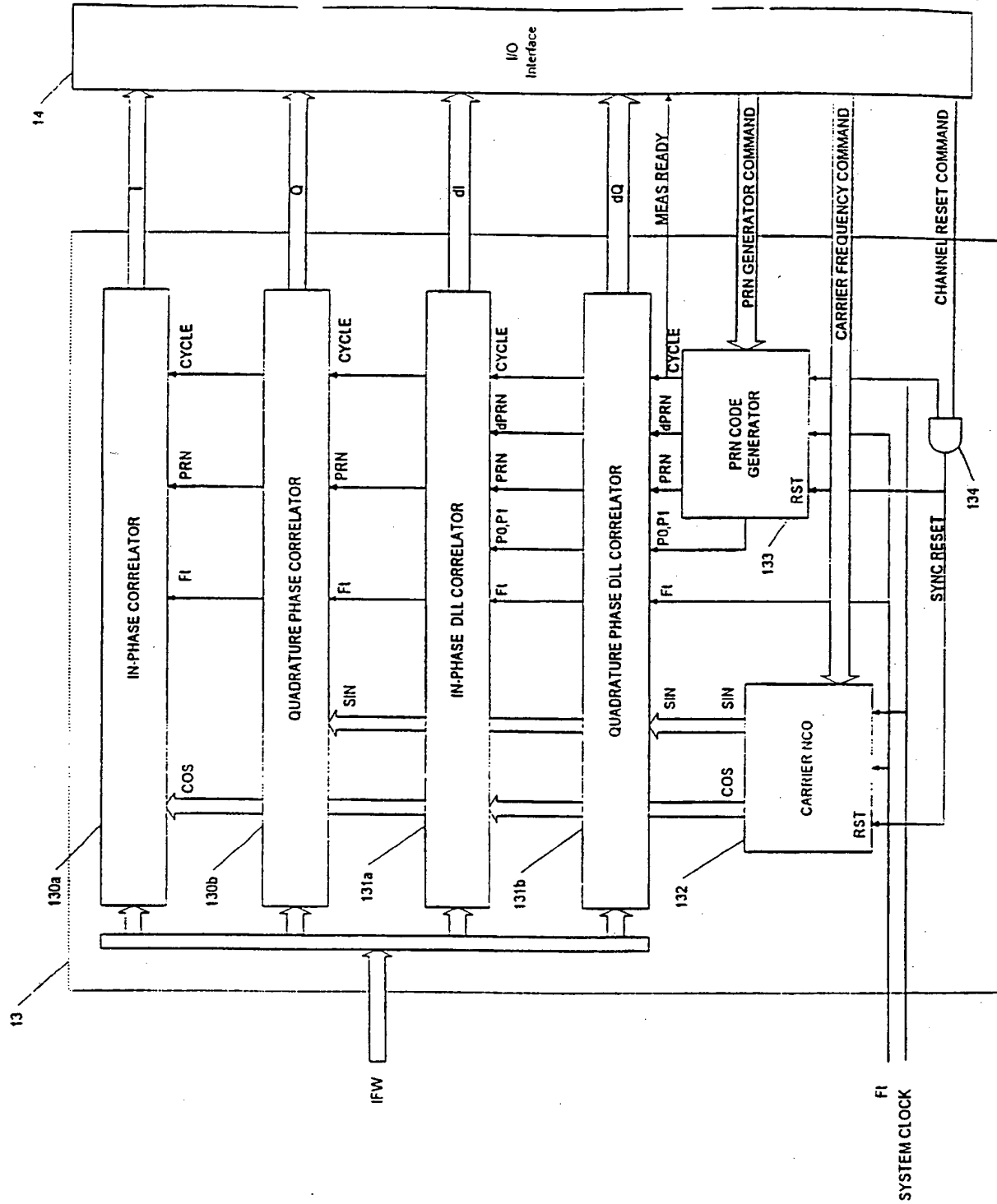


FIG 16
(One Channel)

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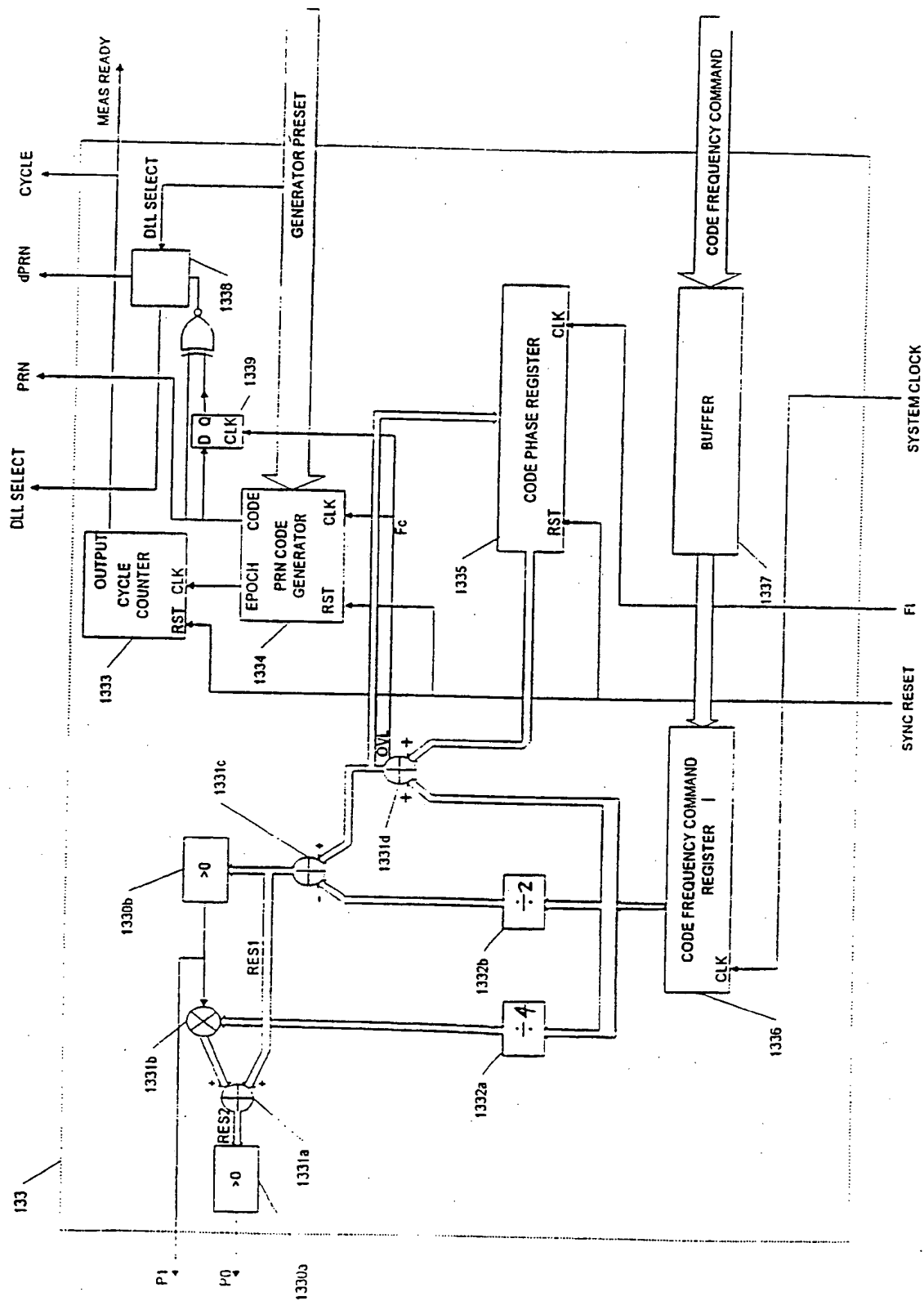


FIG 18
(PAN Code Generator
and Numerically Controlled Oscillator)

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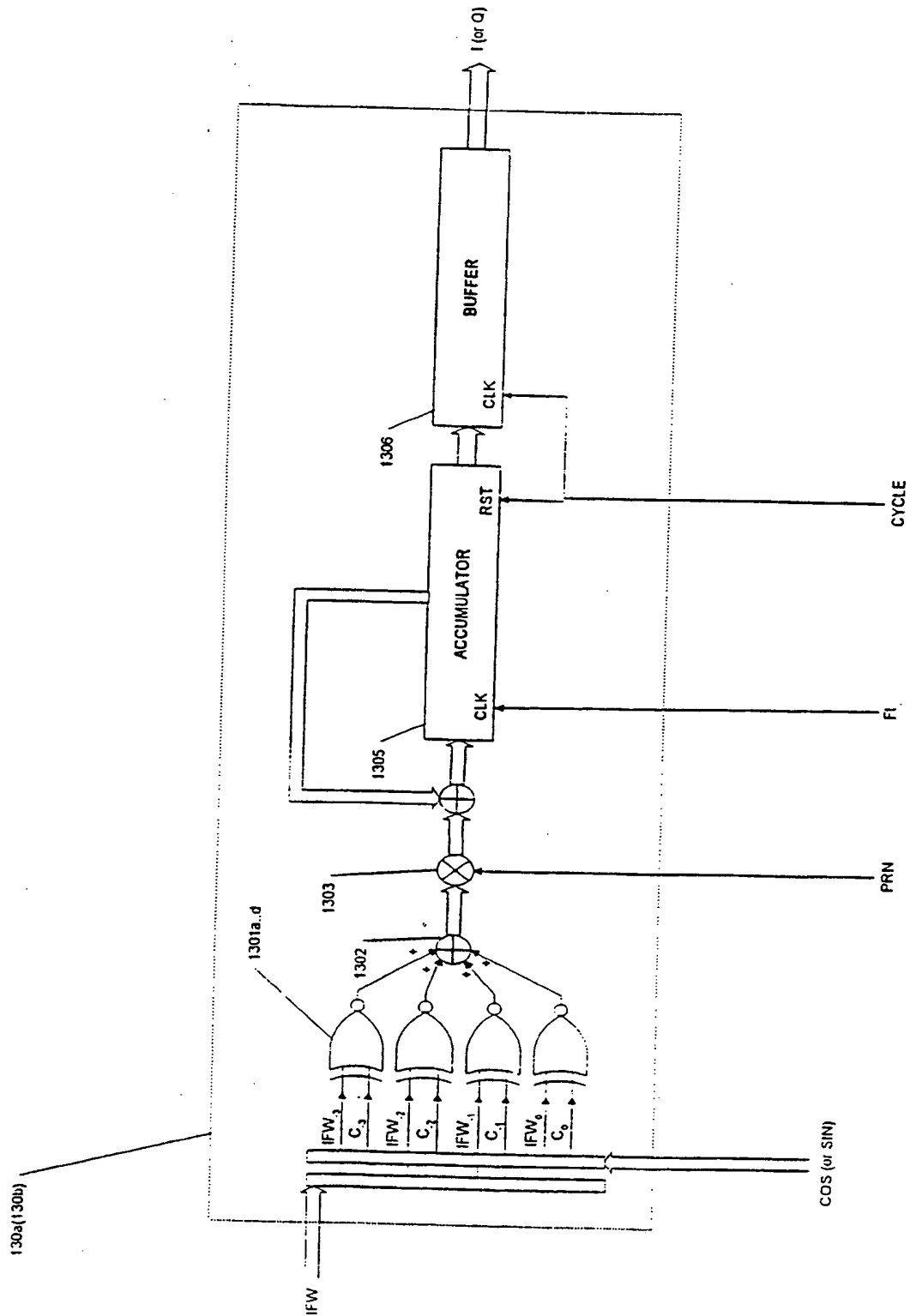


FIG. 19
(Correlator)

2547 = 110

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IASAN No

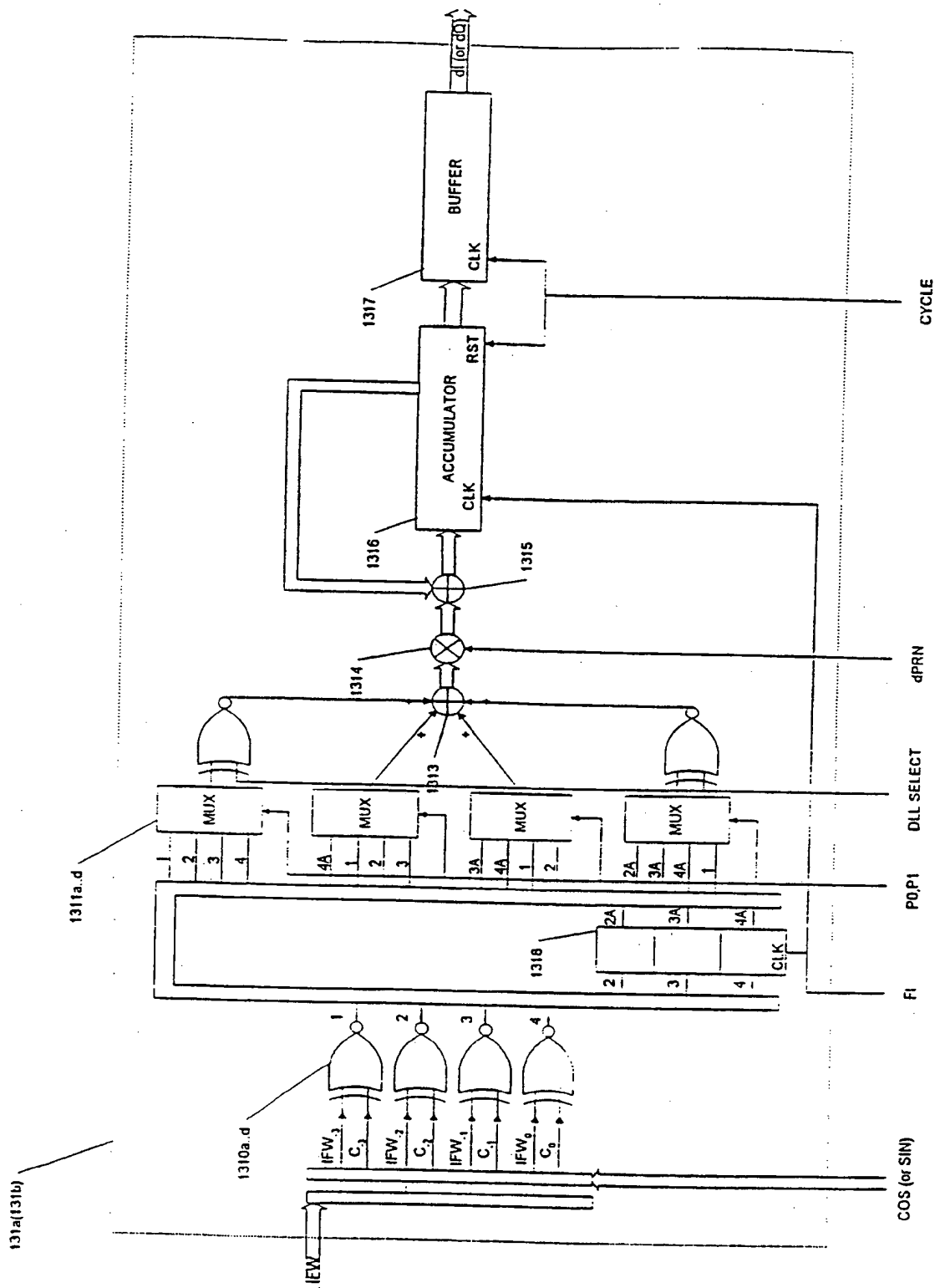
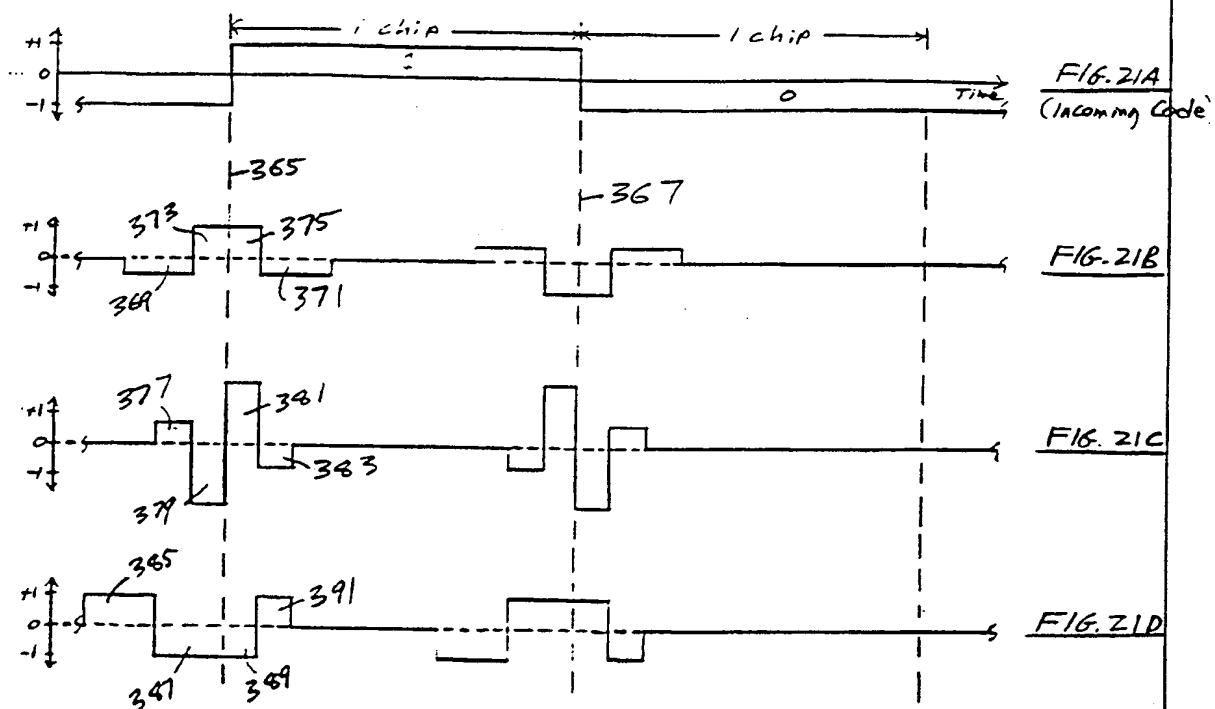


FIG 20

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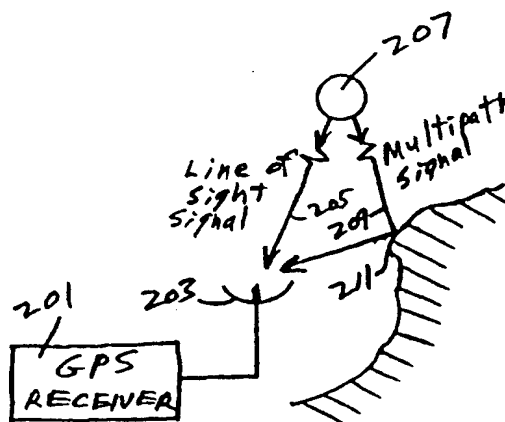
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(71) Applicant: ASHTECH, INC. [US/US]; 1170 Kifer Road, Sunnyvale, CA 94086 (US).			
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(74) Agents: PARSONS, Gerald, P. et al.; Majestic, Parsons, Siebert & Hsue, Suite 1450, Four Embarcadero Center, San Francisco, CA 94111-4121 (US).			
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(54) Title: MULTIPATH ERROR REDUCTION IN A SPREAD SPECTRUM RECEIVER FOR RANGING APPLICATIONS

(57) Abstract

A receiver of a radio frequency signal having a pseudo-random noise (PRN) code, and techniques of processing such a signal that are especially adapted for ranging applications. A signal corresponding to the PRN code is locally generated and used for decoding the received signal in a manner to reduce ranging errors that can result when multipath (delayed) versions of the radio frequency signal are also present. A significant application of the receiver and signal processing techniques of the present invention is in a Global Positioning System (GPS), wherein a number of such signals from several satellites are simultaneously received and processed in order to obtain information of the position, movement, or the like, of the receiver. A delay locked loop (DLL) correlator, provided in each of the receiver's multiple processing channels, locks onto a line of sight signal from one of the satellites with the effect of any multipath signal(s) being significantly reduced.



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INTERNATIONAL SEARCH REPORT

International Application No
PCT/US 96/12967

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According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6 G01S H04B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A E A	<p>EP 0 552 975 A (NOVATEL COMMUNICATIONS LTD) 28 July 1993 see page 3, line 19 - line 34 see page 7, line 54 - line 57 ---</p> <p>WO 96 37789 A (LEICA INC ; STANSELL THOMAS ATLEE JR (US); KNIGHT JERRY EUGENE (US)) 28 November 1996 see page 37, line 4 - page 38, line 24; figure 4 see page 44, line 25 - page 46, line 23; figures 23-25 ---</p> <p>US 5 347 536 A (MEEHAN THOMAS K) 13 September 1994 see the whole document ---</p> <p style="text-align: center;">-/-</p>	<p>9 1,13,16,21 1-3,8-10,13-15,21-23 1,9,13,16,21</p>

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Date of the actual completion of the international search

17 March 1997

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INTERNATIONAL SEARCH REPORT

Int. Patent Application No
PCT/US 96/12967

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INTERNATIONAL SEARCH REPORT

Information on patent family members

Int: ☐ National Application No

PCT/US 96/12967

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(72) Inventors: ZHODZICSHSKY, Mark; Shipilovsky Projezd 41-2-3, Moscow, 11555 (RU). VEITSEL, Victor; Valdajsky Projezd 13-19, Moscow, 125445 (RU). SILA-NOVATISKY, Stanislov; Saltikovskaya Street, 29-3-44, Moscow, 111672 (RU). ASHJAE, Javad; 14403 Sobey Road, Saratoga, CA 95070 (US). GARIN, Lionel; 3475 Greer Road, Palo Alto, CA 94303 (US).

(74) Agents: PARSONS, Gerald, P. et al.; Majestic, Parsons, Siebert & Hsue, Suite 1450, Four Embarcadero Center, San Francisco, CA 94111-4121 (US).

(81) Designated States: AL, AM, AT, AU, AZ, BB, BG, BR, BY, CA, CH, CN, CZ, DE, DK, EE, ES, FI, GB, GE, HU, IL, IS, JP, KE, KG, KP, KR, KZ, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, TJ, TM, TR, TT, UA, UG, UZ, VN, ARIPO patent (KE, LS, MW, SD, SZ, UG), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).

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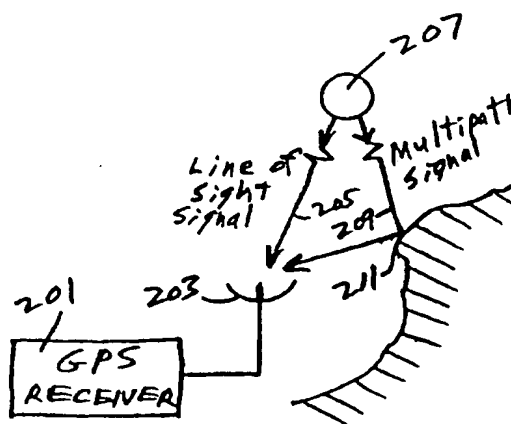
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**MULTIPATH ERROR REDUCTION IN A SPREAD SPECTRUM RECEIVER
FOR RANGING APPLICATIONS**

5

Background of the Invention

10 This invention relates to digital radio
receivers which are used for navigation systems and
other ranging applications, wherein the received signals
are encoded with a pseudo-random noise (PRN) type code.
This invention deals specially with environments where
15 the multipath fading is severe.

 The United States government has placed into
orbit a number of satellites as part of a global
positioning system (GPS). A GPS receiver receives
signals from several such satellites and can determine
20 very accurate parameters, such as position, velocity,
and time. There are both military and commercial uses.
A primary military use is for a receiver in an aircraft
or ship to constantly determine the position and
velocity of the plane or ship. An example of a
25 commercial use includes surveying and the accurate
determination of the location of a fixed point or a
distance between two fixed points, with a high degree of
accuracy. Another example is the generation of a high
accuracy timing reference.

30 In order to accomplish this, each satellite
continually transmits two L-band signals. A receiver
simultaneously detects the signals from several
satellites and processes them to extract information
from the signals in order to calculate the desired

parameters, such as position, velocity or time. The United States government has adopted standards for these satellite transmissions so that others may utilize the satellite signals by building receivers for specific purposes. The satellite transmission standards are set forth in detail by an "Interface Control Document" of Rockwell International Corporation, entitled "Navstar GPS Space Segment/Navigation User Interfaces", dated September 26, 1984, as revised December 19, 1986.

Briefly, each satellite transmits an L1 signal on a 1575.42Mhz carrier, usually expressed as $1540f_0$, where $f_0=1.023\text{Mhz}$. A second, L2 signal transmitted by each satellite, has a carrier frequency of 1227.6 Mhz, or $1200f_0$. Each of these signals is modulated in the satellite by at least one pseudo-random signal function that is unique to that satellite. This results in developing a spread spectrum signal that resists radio frequency noise or intentional jamming. It also allows the L-band signals from a number of satellites to be individually identified and separated in a receiver. One such pseudo-random function is a precision code ("P-code") that modulates both of the L1 and L2 carriers in the satellite. The P-code has a 10.23Mhz clock rate and thus causes the L1 and L2 signals to have a 20.46Mhz bandwidth. The length of the code is seven days; that is, the P-code pattern is begun again every seven days. In addition, the L1 signal of each satellite is modulated by a second pseudo-random function, or a unique clear acquisition code ("C/A code"), having a 1.023Mhz clock rate and repeating its pattern every one millisecond, thus containing 1023 bits. Further, the L1 carrier is also modulated by a 50 bit-per-second navigational data stream that provides certain information of satellite identification, status and the like.

In a receiver, in the process of demodulating those satellite signals, signals corresponding to the known pseudo-random functions are generated and aligned in phase with those modulated onto the satellite signals. The phase of the carriers from each satellite being tracked is measured from the results of correlating each satellite signal with a locally generated pseudo-random function. The relative phase of carrier signals from a number of satellites is a measurement that is used by a receiver to calculate the desired end quantities of distance, velocity, time, etc. Since the P-code encrypted functions (Y-code) are to be classified by the United States government so that they can be used for military purposes only, commercial users of the GPS must work directly only with the C/A code pseudo-random function.

The government of the former USSR has placed into orbit a similar satellite positioning system called GLONASS; more information on its standard can be found in the "Global Satellite Navigation System GLONASS-Interface Control Document" of the RTCA Paper No. 518-91/SC159-317, approved by the Glavkosmos Institute of Space Device Engineering, the official former USSR GLONASS responsible organization. Although the present invention is described herein for use with the United States GPS system, it can be applied to a receiver designed to acquire the GLONASS signals or any radio frequency system using pseudo-random noise sequences for ranging.

One of the major factors influencing the final accuracy of a distance, velocity, etc., measurement being made is the accuracy with which the signal phase measurements are made. In turn, this phase measurement precision is altered if, in addition to the direct line-of-sight propagation signal, a multipath fading signal is also received. The phase of the C/A code, for

example, is determined by use of a delay locked loop (DLL) correlator, wherein the phase of the internally generated C/A PRN code sequence is adjusted in a control loop to minimize an error signal. The DLL uses early and late versions of the internally generated code in a signal correlator that is part of it. Many such receivers use a time spacing between the early and late versions of one PRN code chip. (A "chip" is the time during which the code remains at a plus or minus one.) Operation of the DLL within such receivers is affected by any multipath signal present, thus causing a tracking error. The phase locked condition of the DLL is not only controlled by the line-of-sight signal, as is desired in order to eliminate a cause of phase measurement errors, but rather is affected by the multipath signals as well.

Errors caused by multipath distortion in the out-of-phase condition can be reduced by narrowing the delay spacing between the early and late correlators in the DLL. Although this technique reduces the effect of the received multipath signals somewhat by reducing the loop gain to the weaker multipath signals, inaccuracies still result. The tracking error is never completely eliminated by simply narrowing the early-late delay spacing, no matter what delay in a multipath signal exists.

Therefore, it is a primary and general object of the present invention to further reduce, and even, in some cases, eliminate phase measurement errors that result when one or more multipath versions of a PRN encoded signal are present.

Summary of the Invention

This and additional objects of the present invention are realized, briefly and generally, by providing a DLL correlator having a zero loop gain over

a majority of a range of relative phase difference between the locally generated PRN code and that encoded in the radio frequency signal being received from a satellite or other source, while, at the same time, providing a finite magnitude of loop gain in an operating phase difference region positioned about a zero phase difference. That is, the DLL operates to minimize the error signal for a received signal having a relative phase within a narrow operating phase window and is thus unaffected by multipath versions of that signal which are outside of the window in a region where the loop gain is zero. The present invention exhibits a code loop error which goes practically to zero for far multipath delay, virtually eliminating the influence of the far multipath on the pseudorange measurement accuracy. This improvement is not obtained at the expense of the performances on near multipath, however, in which case the performance is similar to that of the narrow correlator.

In one form of the invention, the radio frequency signal is initially acquired by operating the DLL as a narrow correlator, where there is some gain over the entire range of relative phase differences. After the signal has been acquired by locking the DLL onto a combination of the line-of-sight and multipath signals, the DLL is switched to provide a loop gain in only the small central region, thereby discriminating against the multipath signals.

According to one specific aspect of the present invention, this DLL response is obtained by providing more than one early-late correlator in parallel, with the early-late delays being different. The results of the correlations are arithmetically combined. The size of the central relative phase operating range of the loop response is set by the specific early-late delay values chosen for the

correlators. In the embodiment described hereinafter, two correlators are used, one correlator having an early-late delay of 0.1 chip and the other correlator having a delay of 0.05 chip. During an initial acquisition of the radio frequency signal, only the wider early-late correlator is used.

According to another specific aspect of the present invention, the desired DLL responses are obtained by using specific gating signals in combination with an accumulator/integrator, rather than using early-late versions of the locally generated PRN code. These gating signals are significantly less than one chip in duration and, when in phase with the incoming signal code, occur at each transition of that code between its plus one and negative one values. The gating signals have equal positive and negative areas and have a positive or negative polarity at a center that designates whether the PRN code transition that it represents is positive or negative going. During initial acquisition of the radio frequency signal, the gating signals are shaped as simple positive or negative going pulses occurring at code transitions.

Additional objects, advantages and features of the various aspects of the present invention will become apparent from the following description of its preferred embodiments, which description should be taken in conjunction with the accompanying drawings.

Brief Description of the Drawings

Figure 1 illustrates line-of-sight and multipath signals being received simultaneously by a GPS receiver;

Figures 2 and 3 show the line-of-sight and multipath signals in vector form;

Figure 4 is a general block diagram of a delay locked loop (DLL) correlator;

Figures 5A-5D are curves showing one operation of the circuit of Figure 4;

Figures 6A-6C are curves showing another operation of the circuit of Figure 4;

5 Figures 7 and 8 are block diagrams showing other DLL circuits that are alternatives to that of Figure 4;

Figures 9A-9D are curves which illustrate operation of the DLL circuits of Figures 7 and 8;

10 Figure 10 generally illustrates another type of correlator which uses gating signals for local code generation;

Figures 11A-11D illustrate several ways of operating the circuit of Figure 10;

15 Figure 12 is an enlarged version of a portion of Figure 11D;

Figure 13 shows the results of operating the DLL correlators of Figures 7, 8 and 12 in three different ways;

20 Figure 14 is a block diagram of a complete receiver embodying the various aspects of the present invention;

Figure 15 is a block diagram of the down converter circuit of the receiver of Figure 14, along with timing reference circuitry and sampling;

25 Figure 16 is a block diagram of one channel of the receiver of Figure 14;

Figure 17 shows a carrier numerically controlled oscillator used in each of the channels of Figure 15 in the receiver of Figure 14;

30 Figure 18 shows the PRN code generator of the channel of Figure 16, along with its numerically controlled oscillator;

Figure 19 is a block diagram of the punctual correlator used in the channel circuit of Figure 16;

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Figure 20 is a block diagram of the DLL correlator (in-phase and quadrature phase) used in the channel circuit of Figure 16; and

Figures 21A-21D illustrate alternate gating signals that may be generated in the circuit of Figure 10.

Description of the Preferred Embodiments

Referring to Figure 1, the various aspects of the present invention are described with respect to a global positioning system (GPS). A GPS receiver 201 includes an antenna 203 which is positioned to receive a signal 205 from a satellite 207. In addition to the desired line-of-sight signal 205 received directly from the satellite 207, the antenna 203 also receives a second version of that signal, a delayed multipath signal 209. The multipath signal is delayed because it reaches the antenna 203 by traversing a longer distance than does the line-of-sight signal 205. The multipath signal is shown in Figure 1 to reflect off of a hill 211, or some other object. Although the present invention is explained simply with reference to a single multipath signal, there can be several delayed versions of the line-of-sight signal which are also received by the antenna 203 at the same time. Since GPS receivers, and other ranging receivers used in other applications, operate by measuring the phase of the received signal, a multipath signal can complicate that task considerably.

Various attempts have been made in antenna design to limit the acceptance of reflected signals. This is difficult, however, because it is generally desired to have the antennas maintain a wide angle property in order to receive signals from several satellites at one time that are spread a considerable distance apart. Attempts have also been made to

position the antenna as high as possible, in order to minimize ground and building reflections, or to carefully position it to avoid receiving reflected signals. Although these techniques may be used in conjunction with the present invention, the present invention uses various signal processing techniques within the receiver itself to discriminate against the received multipath signals.

Referring to Figures 2 and 3, a vector 213 represents the received line-of-sight signal, while another vector 215 represents the received multipath signal. The multipath signal 215 arrives at the receiver antenna 203 with a delay τ relative to the line-of-sight signal 213. It is shown in these figures, the multipath signal generally has a lower magnitude than does the line of sight signal as illustrated by its smaller vector 215. A ratio of these magnitudes is noted herein by α .

A delay lock loop (DLL) correlator that is typically used in GPS receivers is shown in Figure 4. A received signal 217 may be radio frequency signal acquired by the antenna 203, after some amplification, but generally is an intermediate frequency signal in a frequency range much lower than that received by the antenna 203. Further, in the GPS receiver environment, a separate such DLL correlator is provided for each satellite signal that is received by the receiver antenna in a single composite signal. One DLL correlator then processes that portion of the incoming signal that emanates from a particular satellite. Further, the signal processing illustrated in Figure 4 is generally done in the digital domain, an analog-to-converter being employed to digitize the incoming intermediate frequency signal. That signal is digitized by a very high frequency sampling clock.

The received signal 217, in whatever form, is mixed in a mixer 219 with a signal 221 that is a replica of the carrier of the received signal 217. This local carrier is generated by an appropriate circuit 223, the phase of the local carrier signal 221 being adjusted by an input control signal 225. A loop circuit to lock the carrier generator 223 onto that of the received signal is not shown in Figure 4 since it can be of a typical design. However, the processing of a signal 227 at an output of the mixer 219 is shown in more detail since it is in this processing where the present invention primarily lies. The signal 227 is the received signal but with its carrier now removed. It is supplied to two mixers 229 and 231 which receive replicas 228 and 230 of a PRN code carried by the received signal. These replicas are, respectively, "early" and "late" in relative phase with respect to a "punctual" replica 245. These replicas come from a local code generator 233 within the receiver. In at least the case of the C/A code in the GPS system, the code carried by the received signal is well known and can be generated within the receivers. The relative phase of the locally generated code is adjusted by a phase control signal 235. Further, in some receivers, another input 237 to the local code generator 233 allows adjustment of the delay between an early and late replicas of the locally generated code.

Outputs of each of the mixers 229 and 231 are applied to appropriate accumulators/integrators 239 and 241, respectively. The outputs of the accumulators 239 and 241 are arithmetically combined in another mixture 243, whose output is an error signal that is applied to the input 235 of the local code generator 233 to adjust its phase. What the loop of Figure 4 is designed to do is to lock the local code generator 233 in phase with the code carried by the received signal 217. Although

this is being described with respect to the C/A code carried by the L1 signals of GPS satellites, the same principles are applicable in a wide variety of applications, particularly in other ranging applications.

It is helpful to refer to the curves of Figures 5A-5D to understand the operation of the DLL correlator of Figure 4. If the punctual output 245 of the local code generator 233 were to be applied to an accumulator of the type of accumulator/integrator 239 or 241, an output characteristic as shown in Figure 5A would result. If this punctual code replica is exactly in phase with the PRN code of the received signal 217, an output of such an accumulator would be a maximum at a center line 247 of the triangular shape output characteristic of Figure 5A. If there is some misalignment in phase between the two, the output of such an accumulator would decrease from such a peak as it travelled down one side or the other of the triangle depending upon whether the local punctual code being generated was delayed or advanced with respect to the PRN code of the received signal.

Although the punctual output of the local code generator 233 is usually used for other purposes in a GPS receiver, the DLL correlator of Figure 4 operates with the early and late versions 228 and 230 of that code. Figure 5B shows the characteristic output of the accumulator 239 from a comparison with the local early code, and the curve of Figure 5C the output function of the accumulator 241 from a comparison with the local late code. In this typical example, the early and late locally generated PRN codes are separated by one chip. That is, the late code 230 is delayed behind the early signal 228 one PRN chip. This fixed delay is designated herein as "d" and is shown in Figure 5B. To state it another way, as shown in relative phase scale along the

x-axis of Figure 5B, the early code function occurs one half a chip in advance of the punctual version, and the late code occurs one half a chip after the punctual version. It is often convenient to reference the early and late correlator outputs, such as shown in Figures 5B and 5C, to a central, in-phase line 247.

Figure 5D shows the error signal 235, resulting from subtracting the correlator function of Figure 5C from that of Figure 5B. The result is a zero error signal at the in-phase point 247 when the local code generator 233 is properly locked onto the PRN code that is part of the received signal 217. As a mismatch in phase occurs, as is well known, the error signal will be driven positive or negative along the curve of Figure 5D. Such an error signal drives the phase of the local code generator 233 in a direction to minimize the error signal, thus keeping the local generator 233 locked onto the incoming signal.

However, if one or more multipath signals are received in addition to the desired line-of-sight signal, the DLL correlator of Figure 4 is influenced by both. This is illustrated in Figure 5D. If only the line-of-sight signal 213 existed, the circuit of Figure 4 would cause it to be aligned with the central zero phase reference line 247. However, because of the multipath signal 215 being received, the local code generator 233 "locks" on a fictitious signal having a phase somewhere around them, as shown in Figure 5D. That is, the circuit of Figure 4 is locking on to an incoming code phase that lies somewhere between that of the line-of-sight and multipath signals. Even though the magnitude of the multipath signal may be low with respect to that of the line-of-sight signal, because of attenuation from reflections of the multipath signal, its effect can be significant because of the steep curve of Figure 5D. It is a combination of the multipath

signal magnitude and the value of the curve at the point of the arrow 215, that determines the level of effect of the multipath signal on this phase lock operation. The line-of-sight signal vector 213 will operate around the in-phase point 247 from that of the multipath signal vector 215. Thus, since measurements with the GPS receiver are largely dependent upon an accurate measurement of the relative phase at the point of the receiver of the C/A code in the satellite signals, this effect of a multipath signal is quite significant to the accuracy of the ultimate measurement.

It has been suggested by others that, in order to reduce the effect of a multipath signal, the delay between the early and late local codes being generated into the receiver should be reduced considerably. An effect of a delay $d=0.1$ chip is shown in Figures 6A-6C. The output of the early accumulator 239 in this case is shown in Figure 6A. Similarly, an output of the late accumulator 241 of Figure 4 is shown in Figure 6B. The error signal output of the adder-subtractor 243 is shown in Figure 6C. It will be noticed that since the amplitude of the error signal function is considerably reduced, the multipath signal 215 has a significantly reduced effect. As can be seen from Figure 6C, the magnitude of the error signal curve at the relative phase of the multipath signal vector 215 is much less than in the example of Figure 5B. The result is that, in a steady state phase lock state shown in Figure 6C, the line-of-sight signal vector 213 is positioned much closer to a desired phase locked position 247 than is the line-of-sight signal.

However, as can be seen from Figure 6C, the DLL correlator of Figure 4 operating with an early-late local PRN code phase difference of one tenth of one chip, the DLL still has not locked on the line of sight signal. An error ϵ is reduced in Figure 6C from Figure

5D but is not eliminated. The multipath signal has an effect in creating this error and thus reducing the accuracy by which a GPS receiver may achieve. According to one aspect of the present invention, the effect of multipath signals is eliminated under certain circumstances and further reduced under other circumstances, by forming a DLL correlator of the type shown in Figure 7 wherein two early-late correlations are arithmetically combined. Referring to Figure 7, an output 227 of the carrier mixer 219 is applied to two correlators connected in parallel. A first correlator includes mixers 251 and 253, the outputs of which are applied to an adder-subtractor 255. An output of the latter mixer is then applied to an accumulator/integrator 257. Similarly, the second correlator includes mixers 259 and 261, the outputs of which are applied to an adder-subtractor 263. An output of that adder-subtractor is applied to and accumulator/integrator 265.

The mixer 251 of the first correlator receives an early code replica 267 from a local code generator (not shown in Figure 7). Similarly, the mixer 253 receives a late code replica 269. The result is an output 271 of the accumulator having a form shown in Figure 9A. The delay between the early and late replicas 267 and 269, respectively, is designated to be d . This is the same as specifying the early signal 267 to be $d/2$ ahead of the central reference phase 279 (Figure 9) and the late local code 269 being $d/2$ behind that reference t . It will be recognized that the output 271 shown in Figure 9A is similar in shape to that of Figure 6C.

Rather than relying simply on that correlator output, however, the second correlator receives in lines 273 and 275 a locally generated code having a difference between the early and late locally generated codes that

is 2d apart. An output 277 of the accumulator 265 is illustrated in Figure 9B. It will be noted that the curve of Figure 9B also generally has the same shape as that of Figure 6C but is different than that of Figure 9A in having a longer slope central portion. This also results in the magnitude in the flat portions of the curve being higher than that of the curve of Figure 9A.

It is in the combination of these two outputs in another adder-subtractor 283 that an error signal 285 of the form illustrated in Figure 9D is obtained. This characteristic is very advantageous since it contains extended portions 287 and 289 where the error signal is zero. This is accomplished, prior to combining the accumulator outputs 271 and 277 in the mixer 283, by reducing the magnitude of the accumulator output 277 by one half with an element 278, resulting in the curve of Figure 9C. This attenuation level is mathematically related to the difference in the widths of the two early-late correlators. The curve of Figure 9C is, in effect, subtracted from that of Figure 9A in the adder-subtractor 283, which gives the desirable error signal characteristic curve of Figure 9D. An operating range 281 exists around the in-phase point 279 wherein the circuit of Figure 7 adjusts the local code generator to drive the error signal of Figure 9D to zero at the in-phase point 279. However, any signal having a relative phase in either of the regions 287 or 289 will not affect the locking of the loop. As shown in Figure 9D, the local code generator can be locked exactly on the line-of-sight signal 213 without any contribution by the multipath signal 215. This occurs so long as the phase delay τ between the vectors 213 and 215, in a fraction of a chip, is greater than that of the operating range 281. Thus, under that circumstance, the effect of the multipath signal on the DLL correlator is completely eliminated.

Because of the wide extent of the zero error signal regions 287 and 289, it can be difficult to initially acquire a signal. That is, when the receiver is first powered up, if the relative phase of the local code generator causes the line-of-sight signal 213 to fall within one of the regions 287 and 289, there will be no error signal to adjust the phase of the local codes being generated. Therefore, a switch 291 (Figure 7) is provided to disconnect the second correlator from the circuit during initial signal acquisition. Thus, during such acquisition, the correlator characteristic output of Figure 9B is non-existent but rather that of Figure 9A. Thus, the multipath signal has some influence during this initial signal acquisition period but it is the purpose of the technique to bring the line-of-sight signal 213 within the operating range 281. Once this occurs, the switch 291 is closed. This then eliminates the influence of the multipath signal. The DLL correlator brings the line-of-sight signal 213 exactly in coincidence with the in phase position 279.

Quantitatively, a $d=0.1$ chip has been found satisfactory. This means that the operating range 281 is 0.1 chip, a very narrow region. In this example, the early - late of the second correlator whose output is illustrated in Figure 9B is twice that of a first correlator whose output is shown in Figure 9A. This results in each of the zero error signal regions 287 and 289 being 0.8 chip in duration, 80% of a possible relative phase difference is between the locally generated code and the PRN code that is part of the signal being received.

There are many variations in the specific parameters that can be selected for operation of the correlator of Figures 7 and 9. The specific early-late phase differences that are chosen for the two correlators may be within a wide range, so long as they

are different, depending upon a particular application and what is desired to be achieved. It is generally preferable, however, that one of the two correlators of Figure 7 have an early PRN code that is one $1/2K$ earlier than the in-phase locked position t , and its late PRN code $1/2K$ after t . Similarly, the second correlator has an early PRN code $N/2K$ ahead of t , and a late PRN code $N/2K$ after t . N and K are integers with N being smaller than K . In the example being described, $N=2$ and $K=10$. If these constraints are followed, the scaling factor of the element 278 of Figure 7 remains at $1/2$. If some other relationship between the two correlators is maintained, that scaling factor will generally need to be something different so that extended zero error signal regions 287 and 289 result when the accumulator output of Figure 9C is subtracted from that of Figure 9A.

Figure 8 shows a modification of Figure 7 wherein four accumulators are used, instead of the two accumulators 257 and 265 of Figure 7. The purpose of Figure 8 is to show that the same result is obtained if the outputs of each of the individual mixers 251, 253, 259 and 261 are accumulated prior to any combination of any of those outputs. An adder-subtractor 293 then receives outputs of the four accumulators, two of which now need to be scaled and switched rather than the single output 277 of Figure 7.

An alternative to the use of early-late correlators, but which gives the same beneficial results, is illustrated in Figure 10. A received signal 301, as previously described with respect to Figures 4, 7 and 8, is applied to a mixer 303 which also receives a replica 305 of the carrier contained in the signal 301. A signal 307, having a local carrier removed, is mixed in a mixer 339 with a gating sequence 341 from a local gating signal generator 343. The mixed signal

output of the mixer 339 is applied to an accumulator/integrator 345 whose output 347 is the error signal that is used to adjust the phase of the output of the local gating signal generator 343 to minimize the error signal.

Operation of the DLL correlator of Figure 10 can be illustrated by reference to the curves of Figure 11. Figure 11A illustrates PRN code that is modulated onto a carrier as part of the received signal 301. The code is a binary one, either being a plus one in level or a negative one in level. One of these levels is chosen to represent a binary bit one, and the other a binary bit zero. Transitions between these levels occur at one chip intervals. The code does not transition between levels every chip, however, but rather its information is contained in the pseudo-random manner in which it stays for one or more chips at one value and then switches to another value for one or more chips, and then back again, and so on.

Figure 11B shows one gating sequence 341 that may be utilized, it having a positive one value at each positive going transition of the incoming code of Figure 11A, and a negative one value at each negative going transition of the incoming code. The gating sequence 341 is zero (Figure 11B) when there is no transition where such a transition is possible. The transition of the gating sequence of Figure 11B coincides with a middle of each chip of the incoming code. The result of using the gating sequence of Figure 11B is an error signal 347 which has essentially the same function as that shown in Figure 5D. That is, the DLL correlator of Figure 10, when its gating sequence 341 is that of Figure 11B, provides essentially the same result as the DLL correlator of Figure 4 with its locally generated early-late PRN codes separated by one chip.

Figure 11C shows a gating sequence 341 which gives an error signal 347 that is essentially the same as that shown in Figure 6C. Coincident with each transition of the incoming code 11A is a pulse having a duration of 0.1 chip. The polarity of the pulse is positive during a positive transition of the incoming code and negative during a negative transition of the incoming code. The width of the pulse can be something other than 0.1 chip, which will then give an error signal function that is something different than that shown in Figure 6C.

Figure 11D shows a local gating sequence according to one aspect of the present invention. Use of this form of the gating sequence 341 (Figure 10) gives an error signal 347 having essentially the same function as that shown in Figure 9D. In order to achieve this, the gating sequence includes, coincident with the occurrence of each transition of the incoming code of Figure 11A, a pulse that has both positive and negative values. The gating sequence 341 is a zero value in between these pulse functions. These pulse functions are considerably less than one chip in duration. Each pulse function has equal positive and negative areas. When phase lock is achieved, a central portion of the pulse function of Figure 11D is aligned with the transition of the incoming code of Figure 11A. If that transition is positive going, then the polarity of the central portion of the pulse function of Figure 11D is of one polarity, and if the incoming code transition is negative going, that pulse function central portion has an opposite polarity. In Figure 11D, it is shown that the central portion at a time 349 coincident with a positive going edge of the incoming code of Figure 11A is positive, and that the pulse function central portion at a time 351 coincident with

a negative going edge of the incoming code of Figure 11A is negative, but these may be reversed.

Referring to Figure 12, characteristics of the pulse functions of Figure 11D will be explained with respect to the expanded scale diagram. A single pulse function occurring about the incoming code transition 349 can be viewed as having four distinct adjacent components. A central portion of the pulse function have areas 353 and 355 that are equal in area to each other on opposite sides of the transition line 349 when the error signal of the correlator of Figure 10 is minimized. Areas 357 and 359 have an opposite polarity to areas 353 and 355 and occur, respectively, ahead of and behind the pulse function areas 353 and 355. The areas 353 and 357 are caused to equal each other. Similarly, the areas 355 and 359 are caused to equal each other. In the specific example being described, the areas 353 and 355 have a width of 0.1 chip with a plus 1 magnitude while each of the areas 357 and 359 has a width of one half that or 0.05 chip, with a minus one magnitude.

Referring to Figure 13, curves are given to illustrate the relative tracking error boundaries for various multipath signals having different values of delay from the line of sight signal desired to be locked onto. The outer-curves 361 and 363 show the results of operating the DLL correlator of Figure 4 in a manner described with respect to the curves of Figure 5. The dashed lines 365 and 367 illustrate operation of the DLL correlator of Figure 4 in accordance with the curves of Figure 6, as described previously. It can be seen that the tracking error is considerably reduced but still is significant. A curve 369 of Figure 13 shows how the error is considerably reduced when one of the DLL correlators of Figures 7 or 8, as explained with respect to the curves of Figure 9, is utilized. The same

result, illustrated by the curve 369, occurs by using the gating sequence of Figure 11D with the correlator of Figure 10, as previously described. It will be noted from the curve 369 that multipath signals which are
5 delayed from the line of sight signal by any significant amount do not affect the tracking at all.

More specifically, Figure 13 shows in nanoseconds (ns) the envelope of zero tracking error for the three DLL correlators Θ versus the delay τ in ns,
10 for a ratio α of the magnitude of the multipath signal to that of the line-of-sight signal is 0.5 with Θ varying between $-\pi$ and $+\pi$. It is obvious that for τ between 0 and 10ns, the zero tracking error is roughly identical for the three correlators, and for τ around
15 100ns the advantage is clearly in favor of the 0.1 chip edge DLL. After 150ns, the zero tracking error becomes negligible for the $d=0.1$ chip edge correlator, whereas it stays at 30ns in the narrow correlator and above and increasing for the 1 chip wide correlator.
20 Conceptually, the edge DLL correlator used on C/A code is equivalent to a DLL correlator used on P code, and has the same beneficial multipath mitigation properties.

Embodiment of a GPS Receiver

The following description is mainly oriented
25 towards the United States' Global Positioning System (GPS); however it can also be applied to the Common Independent States' GLObal NAVigation Satellite System (GLONASS) as well, or to any ranging system using a PRN sequence. This embodiment is described with one bit
30 quantization; this choice, made for the sake of the simplicity of the description, does not preclude any constraint on the quantization.

Referring to Figure 14, a general block diagram of a pseudo-random noise (PRN) receiver 10 that
35 implements the present invention. The receiver 10

includes an antenna 11, a downconverter 12, multiple channels 13a to 13n, an input/output interface 14, and a digital processor 15. The antenna 11 receives a composite signal RF, composed of signals from all satellites in the system that are directly in the line of sight of the antenna. The composite signal RF is fed to the down-converter 12 to provide a quantized and sampled intermediate frequency signal IFW, a system sampling clock F_t and a SYSTEM CLOCK.

The signal IFW is a word of 4 bits, each representing one of four IF consecutive samples at a F_s sampling rate. The processing clock F_t is a division by 4 of the F_s signal. The system clock is a further division of F_t signal, interrupting the processor at a rate of approximately 1 per millisecond and triggering the channel processing.

Referring to Figure 15, the down-converter is discussed. The RF signal is first prefiltered by the RF filter 120, amplified by 121, and mixed with the Local Oscillator (LO) by the mixer 122, filtered and amplified again in IF by 123 and 124, and finally quantized in one bit by the hard limiter 125. The filter 123 is in fact used as a pre-correlation filter with a two-sided bandwidth of 20.46Mhz. The instantaneous hard limiter output is sampled at a rate of F_s , and shifted in the 4-stage shift register 126. The sampling rate F_s is chosen to satisfy the Nyquist rate requirement, related to the pre-correlation filter bandwidth. Every F_t clock transition (i.e. 4 F_s clocks), the full contents of the shift register is transferred into a parallel register 127. The 4 bit word IFW is then transferred to the channel circuits at a F_t rate for satellite individual tracking.

The clock reference circuitry of the down converter (Figure 15) includes a phase lock loop (PLL) which is composed itself of the voltage controlled

oscillator (VCO) 131, a frequency divider 132, a phase comparator 129, which compares the phase with a stable reference oscillator 128, and, finally, a low frequency loop filter 130. The VCO output is used as local oscillator for the RF section. The frequency of the VCO 131 is divided in several steps, a first time by a divider 133 to get the sampling frequency F_s , a second time by a divider 134 to get the processing clock F_t , and a third time by a divider 135 to get the SYSTEM CLOCK.

As shown in Figure 14, the sampled and quantized intermediate frequency signal IFW is simultaneously fed to each of the several signal processing channels 13a to 13n. A separate channel 13 is devoted to every visible satellite; the assignment to a given satellite is made by configuring the pseudo-random noise (PRN) generator through the PRN GENERATOR COMMANDS. The structure of a channel 13, typical of each of the channels 13a-13n, is given in Figure 16. Every satellite signal is simultaneously tracked in carrier phase by a carrier Phase Lock Loop (PLL) and in code phase by a Delay Lock Loop (DLL). All channel processing is made in a fully synchronous manner at a processing clock F_t . IFW samples are processed 4 by 4, and all carrier and code generation is made at F_t rate by groups of 4 as well.

Both the PLL and the DLL are implemented partly in the channel 13, and partly in the processor 15. The link is made by the I/O interface 14. The loop comparators and the loop actuators are located in each channel, whereas the filter implementation and the loop management are handled by the processor 15. The loops are updated when the processor is interrupted by the SYSTEM CLOCK signal and the MEAS READY signal is set for that channel, informing the processor that a measurement cycle has just finished. All measurement cycles are

chosen at a period bigger than that of the SYSTEM CLOCK, in order not to miss any measurement. The cycle period is set by the processor at every channel initialization, through the PRN GENERATOR COMMAND.

5 The carrier PLL uses the measurements I and Q of an in-phase correlator 130a, and a quadrature phase correlator 130b. In a tracking mode, the PLL drives the information Q to zero while checking for the presence of the signal locking on I. Both correlators are using the
10 same "punctual" pseudo-random code (PRN) for the correlation, but use different carrier signals COS and SIN. The processed information is used to control the CARRIER FREQUENCY COMMAND of a carrier numerically controlled oscillator (NCO) 132.

15 The carrier NCO 132 is described in detail in Figure 17. The instantaneous carrier phase image is kept in a carrier phase register 1325, where the total range represents 2π of carrier phase. The current CARRIER FREQUENCY COMMAND is kept in a frequency command
20 register 1323. At every Ft transition, this value is added to the current carrier phase register contents by the adder 1321c; thus, the carrier phase is incremented one full cycle every time the carrier phase register 1325 cycles back to zero.

25 The instantaneous carrier phase can be obtained at any SYSTEM CLOCK transition or at every Ft very straightforwardly; the carrier phase register 1325 is reset synchronously with the SYSTEM CLOCK at the initial CHANNEL RESET command, ensuring a known initial
30 phase. Every processor command loaded into a buffer 1324 is transferred into the frequency command register 1323 and effective at the next SYSTEM CLOCK transition; as the SYSTEM CLOCK period is an exact number of Ft periods and knowing the loaded command word, the exact
35 value in the carrier phase register is obtained at the

next SYSTEM CLOCK transition or at any Ft clock transition in between by direct computation.

The one bit reference carrier cosine value C_0 is obtained by "exclusively ORing" the most significant bit (MSB) and the second most significant bit of the carrier phase register contents. The one bit reference carrier sine value is obtained using the MSB of carrier phase register contents; this is actually done in the phase/quadrature signal generator 1320c.

As the samples are processed 4 by 4, the carrier references are generated synchronously with the exact sampling times for the 3 other samples as well. Arbitrarily and for simplicity of implementation, the reference signal is chosen to be the third of the sequence of 4.

If may be noted that the carrier phase 1325 is physically incremented by the frequency command value 1323 every Ft. It is equivalent to say that the instantaneous carrier phase is virtually incremented by a fourth of this value every Fs (i.e. four times per Ft period). As a result, the reference carrier phase synchronous with the fourth sample (most recent one) is obtained by adding frequency command divided by four (divider 1322c) to the current carrier phase 1325; the carrier cosine (sine) value C_{-1} (S_{-1}), delayed of one sampling period, is obtained from it with the phase quadrature signal Generator 1320d using the same algorithm as for C_0 and S_0 .

Similarly, C_{-2} , S_{-2} are obtained by subtracting frequency command value divided by 2 using 1322a from the current carrier phase 1325. This subtraction is performed by using the adder 1321a. The cosine and sine values are finally obtained through 1320a.

Finally C_{-1} , S_{-1} are obtained by subtracting the frequency command value divided by 4 using 1322b from the current carrier phase 1325. This subtraction is

made using the adder 1321b. The cosine and sine values are finally obtained through 1320b.

The full NCO output is a "cosine" word COS and a "sine" word SIN of 4 bits each, each bit being the sampled carrier reference value one sample apart. The "punctual" in-phase (130a) and quadrature-phase (130b) correlators for the PLL are described in Figure 19. Given the close similarity, the following correlator description deals with only the in-phase case.

The intermediate frequency word IFW composed of 4 samples is "exclusive ORed" with the 4 bit cosine carrier reference COS in the structure 1301a to 1301d. All samples are added in the adder 1302; the result is comprised between -4 and +4 (the "0" values are processed as "-1" by the adder 1302). The result is then multiplied by the value of reference PRN sequence synchronous with the most recent sample (multiplier 1303). The resulting value is then algebraically added at a Ft rate to the current contents of the accumulator 1305. At every CYCLE transition the accumulator value is transferred to the buffer, the accumulator is reset, and finally a new measurement period is initiated. The processor is then able to read the measurement values to close the loops.

Going briefly back to Figure 16, the delay lock loop will be described in more detail. The DLL has 2 configurations, acquisition mode or tracking mode, depending on the channel locking phase. As described in the prior section, the tracking mode preferably uses an "edge DLL" correlator, while the acquisition mode uses a 0.1 chip delay DLL. The selection between 2 modes is made through the signal DLL SELECT. Other specific combinations of tracking and acquisition mode correlators may also be employed.

The delay lock loop (DLL) processing is timed at a Ft rate similarly to the PLL, and the measurement

update rate is CYCLE as well. The DLL uses dI and dQ information coming from an in-phase DLL correlator 131a for dI, and a quadrature phase DLL correlator 131b for dQ. The DLL drives the dQ value to zero when in tracking mode. The dQ is used in conjunction with dI when in acquisition mode. The processed information is used to control the PRN GENERATOR COMMANDS of the PRN Code Generator 133.

The "edge DLL" principle, previously described with respect to Figures 10, 11D and 12, will be described in more detail, in light of the GPS receiver just described. For "edge DLL" implementation purposes, four time intervals of equal duration have to be defined around the PRN code transition; two before the code transition and two after. In the current embodiment, each time interval has an exact duration of $1/F_s$ or the IF sampling period.

We thus infer that every time interval contains one and only one IF sample at a F_s rate. The relative position of the samples in the interval is unknown and depends on the relative phase between code generator and sampling clock. The full formula expressing the DLL response is given below.

Assume that $S_{-2}, S_{-1}, S_{+1}, S_{+2}$ is a sequence of four consecutive IF samples with the code transition between S_{-1} and S_{+1} , and the associated sampled PRN code

sequence is $PRN_{-2}, PRN_{-1}, PRN_{+1}, PRN_{+2}$ (with $PRN_{-2} = PRN_{-1}$ and $PRN_{+1} = PRN_{+2}$). $dPRN$ may be defined as:

$$dPRN = \frac{1}{2} \cdot (PRN_{+1} - PRN_{-1})$$

Thus $dPRN$ equals:

- +1, if the transition is a rising edge,
- 1, if the transition is a falling edge,
- 0, if two consecutive PRN chips are identical.

$dPRN$ can be thought as the derivative of the PRN sequence.

At every PRN chip code transition, the elementary DLL contribution is given by:

$$DLL_i = (-S_{-2} + S_{-1} + S_{+1} - S_{+2}) \oplus dPRN$$

The contribution is not zero if $dPRN \neq 0$ (i.e. if $PRN_{-1} \neq PRN_{+1}$).

After an integration period defined between two contiguous CYCLE transitions, the full DLL response will be:

$$DLL = \sum_i DLL_i$$

This summation performs a low pass frequency filtering function of the measurements dI and dQ .

Going back to the physical implementation, we notice that knowing a code transition falls inside a

group of 4 IFW samples, we still have to know between which samples of the group the code transition falls. The signals P0 and P1 show where the code transition falls among the 4 IFW samples. Because we need to add 4 consecutive values and the code transition can have 4 different positions in the sequence, we need to keep the 3 previous samples of the previous sequence of 4 IFW. The total sequence will be, from the oldest sample to the newest: S_{2A} , S_{3A} , S_{4A} , S_1 , S_2 , S_3 , S_4 and PRN, being the PRN code synchronous with S_4 .

P1 value	P0 value	code transition falls between	Elementary DLL operation in tracking mode	Elementary DLL operation in acquisition mode
0	0	S_{3A} and S_{4A}	$(-S_{2A} + S_{3A} + S_{4A} - S_1) \odot \text{PRN}$	$(+S_{2A} + S_{3A} + S_{4A} + S_1) \odot \text{PRN}$
1 5 0	1	S_{4A} and S_1	$(-S_{3A} + S_{4A} + S_1 - S_2) \odot \text{PRN}$	$(+S_{3A} + S_{4A} + S_1 + S_2) \odot \text{PRN}$
1	0	S_1 and S_2	$(-S_{4A} + S_1 + S_2 - S_3) \odot \text{PRN}$	$(+S_{4A} + S_1 + S_2 + S_3) \odot \text{PRN}$
1	1	S_2 and S_3	$(-S_1 + S_2 + S_3 - S_4) \odot \text{PRN}$	$(S_1 + S_2 + S_3 + S_4) \odot \text{PRN}$

Table 1

20

Going to Figure 20, the implementation of the In-Phase DLL correlator 131a is described in detail. After multiplying IFW by the Carrier word COS by 1310a to 1310d, the three last samples of the current IFW word are latched in 1318. At the input of the four multiplexors 1311a to 1311d, seven samples are simultaneous available, S_1 to S_4 from the current IFW and S_{2A} to S_{4A} from the preceding one. Depending on the current value of P1 and P0, a common selection is made on all 4 multiplexors. For the remaining of the explanation, we will assume that $P0=P1=0$. On 1311a output, S_1 is available; on 1311b, S_{4A} is available, and so on. The adder 1313 adds up all selected samples (interpreting "0" inputs as "-1" value in the process). The result is then multiplied by dPRN to form the elementary value DLL_1 . In tracking mode, the signal DLL

35

SELECT will invert the values coming out from the first and the last multiplexor, thus fully implementing the tracking DLL formula described in the first line of the Table 1.

5 The current value between +4 and -4 is algebraically added to the accumulator 1316 by the adder 1315 during the same Ft transition. Every transition on CYCLE transfers the accumulator value to the buffer 1317, resets the accumulator, and finally initiates a
10 new measurement period.

 There is only a slight difference when implementing the acquisition mode. The circuitry is identical up to the adder 1313, except that the first and last sample coming out from the multiplexor 1311a
15 and 1311d are not inverted. The dPRN signal is defined the same way than previously, but its size is expanded to reach 0.1 code chip duration, centered on the code transition.

 Referring to Figure 18, the full PRN code
20 generator will be described. The Generator is in fact composed of a code numerically controlled oscillator (NCO), which delivers a chip frequency clock Fc whose frequency is in direct control of the processor through the CODE FREQUENCY COMMAND; in turn, Fc clocks the PRN
25 code generator 1334 per se.

 Let's begin by the Code NCO description: similarly to the carrier NCO, it is embodied by a code phase register 1335, whose full range represents 2π of the code phase. At every Ft transition, the word into
30 code frequency command register 1336 is added (modulo the range of code phase register) to the contents of the code phase register by the adder 1331d. The carry signal coming from the adder is used as chip frequency Fc. The CODE FREQUENCY COMMAND word present in the code
35 frequency command register is loaded at every SYSTEM CLOCK transition from the buffer 1337. The buffer is

itself loaded from the processor at any time. Another important function of the code NCO is to deliver the signals P0 and P1, whose function was described earlier.

The P0 and P1 signals are generated as follows: if R is the total range of the code phase register (CPR) 1335, and $\Delta\phi$ is the phase increment at every F_s sample ($\Delta\phi = \text{CODE FREQUENCY COMMAND} / 4$).

	$0 < \text{CPR} \leq \Delta\phi$	$\Delta\phi < \text{CPR} \leq 2\Delta\phi$	$2\Delta\phi < \text{CPR} \leq R - 2\Delta\phi$	$R - 2\Delta\phi < \text{CPR} \leq R - \Delta\phi$	$R - \Delta\phi < \text{CPR} \leq R$
P1	0	0	1	1	1
P0	1	0	0	1	0

Table 2

P1 is obtained by subtracting the Code Frequency Register (CFR) 1336 divided by two (by divider 1332b) from the Code Phase Register (CPR) 1335 by use of the adder 1331c. If the result RES1 is positive, P1 = 1.

The P0 case is different depending on the P1 value. If P1 is zero ($\text{CPR} < 2\Delta\phi$), CFR, divided by four (by divider 1332a), is multiplied by -1 in the multiplier 1331b; if P1 is one ($\text{CPR} \geq 2\Delta\phi$), $\text{CFR}/4$ is multiplied by +1. Then 1331a adds RES1 to the multiplication result; the carry of the adder 1331a is taken as P0. The final result is in agreement with Table 2.

The PRN code generator 1334 is clocked by the chip frequency F_c . It is configured for a particular satellite sequence by the command GENERATOR PRESET. It outputs an epoch signal, synchronous with a particular instant in the PRN sequence, which is taken as reference in the PRN ranging sequence. The data bits superimposed on the PRN sequence have their transition perfectly synchronous with this epoch signal.

The EPOCH signal clocks the cycle counter 1333, which is reset at the initialization of the channel by the SYNC RESET, and counts an integer number of epochs (preset at the preset sequence) before to
5 generate a transition on CYCLE, which stops the current measurement cycle on all correlators and informs the processor by the signal MEAS READY. Every channel has its own cycle counter, synchronized on its own data transitions. After a synchronizing phase on the data
10 transitions, it is possible to slow down the measurement periods up to 20ms, no data transitions occurring during this period.

It is assumed, accurately, that the edge DLL correlator used on C/A code, with a precorrelation
15 bandwidth prefiltering (typically 20.46Mhz double sided) improves the multipath error. A PRN code transition detector is built X-ORing the current code output and the previous one latched in the latch 1339. The signal dPRN is generated by 1338 according to the
20 description in the DLL principle explanation.

According to the usual multipath model, the direct received signal is given by:

$$A \cdot PRN(t) \cdot \cos(\omega_0 t + \varphi)$$

where:

A is the amplitude of the received signal

25 PRN(t) is the pseudo-random sequence

ω_0 is the carrier frequency pulsation

φ is the carrier phase offset

The multipath signal is given by:

$$A \cdot \alpha \cdot PRN(t - \tau) \cdot \cos(\omega_0(t - \tau) + \phi - \theta)$$

where:

α is the amplitude ratio between direct and multipath signal

5 τ is the propagation delay between direct and multipath signal

θ is the additional phase rotation between direct and multipath signal.

10 The main effect of the presence of a multipath signal is to shift the zero crossing of the DLL response from the "zero multipath" reference differently for each of the three discriminators. The DLL driving the DLL correlator output to zero in average, the difference between zero crossings will be seen directly as an error in the measured code phase. As the different satellites on which the channels do not experience the same multipaths because of a different geometry, the position computation will be erroneous.

20 Returning to the above description, with respect to Figures 11D and 12, of operation of a receiver that uses the demodulation technique of Figure 10, a few alternate local gating sequences will be described. Figures 21B, 21C and 21D give other examples of what the gating signal generator 343 can provide in line 341. The result in terms of the error signal characteristic of Figure 9D is substantially the same, but the different gating sequences of Figures 21B-D cause the height and duration of the non-zero portions of the Figure 9D curve to change somewhat. The fundamental advantage is retained, however, of providing
30 extended intervals where the error signal is zero.

In each of Figures 21B-D, a carefully controlled gating signal occurs at each of transitions 365, 367, etc., of the incoming code (Figure 21A). In Figure 21B, negative portions 369 and 371 of the signal have a magnitude less than 1, while corresponding positive portions 373 and 375 have a magnitude of 1. The lower magnitude negative portions of the signal are given longer durations, however, so that the areas of the pulse portions 369 and 373 are equal, as are the areas 371 and 375. In the gating signal of Figure 21C, a positive area 377 (magnitude less than 1) is much smaller than a negative area 379 (magnitude more than 1), while a positive area 381 is much smaller than a negative going area 383. This gating signal differs from the others shown herein by aligning with the code signal edge 365 (when a minimum error condition exists) a transition between negative and positive going portions of the signal. Each of the signals of Figures 11D, 12, 21B and 21C is symmetrical about the code edge. The signals are positioned with their middle aligned with the code edge.

In Figure 21D, however, the gating signal is non-symmetrical about the incoming code edge. But the positive and negative going pulse portions have equal areas on each side of the code edge. That is, areas 385 and 387, on one side of the code edge 365, are substantially equal, while the areas 389 and 391 on the other side of the code edge 365 are also substantially equal.

Although several specific examples of compound gating pulse shapes have been given, there are numerous other shapes, with various relative magnitudes, that can be employed instead. The total negative and positive going areas of any such compound gating pulse is made to be substantially equal. This property causes the multipath signal to be substantially eliminated so long

as its delay from the line of sight signal is sufficient.

5 Although the various aspects of the present invention have been described with respect to their preferred implementations, it is understood that the invention is protected within the full scope of the appended claims.

IT IS CLAIMED:

1. A method of decoding an incoming signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, comprising:

locally generating a PRN signal corresponding
5 to the PRN code of the incoming signal,

mixing the locally generated PRN signal with the incoming signal,

developing, from a result of mixing the locally generated PRN signal with the incoming signal,
10 an error signal having a magnitude as a function of a relative phase difference between the incoming signal PRN code and the locally generated PRN signal that (a) is zero for a zero relative phase difference and for a majority of a range of the relative phase difference
15 between plus and minus one chip, and (b) increases as the relative phase difference changes from zero to another value within a central portion of said range, and

when the error signal has a non-zero magnitude
20 within said central portion of said range, adjusting said relative phase difference by adjusting the phase of the locally generated PRN signal a manner to drive the error signal to zero, thereby to drive the relative phase difference between the incoming signal PRN code
25 and the locally generated PRN signal to zero.

2. The method of claim 1 wherein the local generation of the PRN signal corresponding to the PRN code of the incoming signal includes generating an operating set of recurring non-zero gating signals
5 representing edges of the PRN code and which individually (a) are less than one chip in duration, (b) have equal positive and negative areas, and (c) have a positive or negative polarity at a center thereof

corresponding to whether a PRN code edge is positive or
10 negative going.

3. The method according to claim 2 wherein,
prior to locally generating said operating set of gating
signals, an initial set of non-zero recurring gating
signals are generated with recurring non-zero gating
5 signals that individually (i) are less than one chip in
duration, and (ii) have a single positive or negative
polarity that designates whether a PRN code edge is
respectively positive or negative going, thereby to
initially acquire an incoming signal before locally
10 generating the operating set of gating signals.

4. The method according to claim 1 wherein
the local generation of the PRN signal corresponding to
the PRN code of the incoming signal includes generating
as an operating set of PRN signals a first replica
5 advanced in phase $1/2K$ of said chip with respect to a
reference, a second replica delayed in phase $1/2K$ of
said chip with respect to said reference, a third
replica advanced in phase $N/2K$ of said chip with respect
to said reference, and a fourth replica delayed in phase
10 $N/2K$ of said chip with respect to said reference,
wherein N and K are integers with N being smaller than
 K .

5. The method according to claim 4 wherein
mixing of the incoming signal with the first, second,
third and fourth locally generated PRN code replicas
results in corresponding first, second, third and fourth
5 mixed signals, and wherein developing the error signal
includes giving the first and fourth mixed signals the
same polarity that is different from a common polarity
of the second and third signals.

6. The method of claim 4, wherein K equals 10 and N equals 2.

7. The method of claim 4 wherein, prior to locally generating the operating set of PRN signals, an initial set of PRN signals is generated that includes said first and second replicas without said third and fourth replicas, thereby to initially acquire an incoming signal before locally generating the operating set of gating signals.

8. The method of any one of claims 1-7 wherein the incoming signal includes at least a primary signal being received directly in a line of sight from a transmitter and a multipath version of the primary signal being received with a phase delay therebetween that is greater than said central portion of the error signal range, whereby the adjusting of the relative phase difference is performed with respect to the primary signal and not the multipath signal.

9. In a receiver of a radio frequency signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, a method of locking onto the PRN code of a primary signal received in a line of sight from a transmitter when a multipath version of that signal is also received with a time delay of a fraction of one chip, comprising:

generating a PRN signal corresponding to the PRN code of the received signal,

10 mixing the generated PRN signal with the received signal which includes both the primary signal and the delayed multipath version thereof,

adjusting a relative phase of the generated PRN signal in response to an error signal, and

15 initially generating the error signal from
 comparing the phase of the generated PRN signal with the
 phase of a composite of the primary and multipath
 signals, and then subsequently generating the error
20 signal from comparing the phase of the generated PRN
 signal with the phase of the primary signal without the
 multipath signal.

 10. The method of claim 9 wherein the
 generation of the PRN signal includes generating an
 operating set of recurring non-zero gating signals
 representing edges of the PRN code and which initially
5 (i) are less than one chip in duration, and (ii) have a
 single positive or negative polarity that designates
 whether a PRN code edge is respectively positive or
 negative going, and then subsequently (a) are less than
10 one chip in duration, (b) have equal positive and
 negative areas, and (c) have a positive or negative
 polarity at a center thereof corresponding to whether a
 PRN code edge is positive or negative going.

 11. The method according to claim 9 wherein
 the generation of the PRN signal includes initially
 generating a first replica advanced in phase $N/2K$ of
 said chip with respect to a reference and a second
5 replica delayed in phase $N/2K$ of said chip with respect
 to said reference, and then subsequently adding a third
 replica advanced in phase $1/2K$ of said chip with respect
 to said reference and a fourth replica delayed in phase
10 $1/2K$ of said chip with respect to said reference,
 wherein N and K are integers with N being smaller than
 K .

 12. The method of claim 11, wherein K equals
10 and N equals 2.

13. A method of decoding an incoming signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, comprising:

5 locally generating recurring non-zero operating gating signals representing PRN code edges and which individually (a) are less than one chip in duration, (b) have equal positive and negative areas, and (c) have a positive or negative polarity at a center thereof that designates whether a PRN code edge is
10 positive or negative going,

mixing the incoming signal with each of the locally generated gating signals, thereby generating first and second mixed signals,

15 correlating and accumulating said first and second mixed signals, thereby obtaining a correlation signal, and

20 using the correlation signal to adjust the phase of the locally generated gating signals with respect to the PRN code of the incoming signal in order to maximize the correlation, thereby to lock the phase of the locally generated gating signals to the phase of the PRN code in the incoming signal.

14. The method according to claim 13 wherein, prior to locally generating said operating gating signals, generating an initial gating signals with recurring non-zero gating signals that individually (i)
5 are less than one chip in duration, and (ii) have a single positive or negative polarity that designates whether a PRN code edge is positive or negative going.

15. The method according to claim 13 wherein the individual gating signals have a common duration in terms of a fraction of a chip of the PRN code of the incoming signal.

16. A method of decoding an incoming signal containing a carrier having encoded thereon a pseudo-random noise (PRN) binary code, comprising:

5 locally generating replicas of the incoming signal PRN code including a first replica advanced in phase $1/2K$ of said chip with respect to a reference, a second replica delayed in phase $1/2K$ of said chip with respect to said reference, a third replica advanced in phase $N/2K$ of said chip with respect to said reference,
10 and a forth replica delayed in phase $N/2K$ of said chip with respect to said reference, wherein N and K are integers with N being smaller than K ,

mixing the incoming signal with the locally generated PRN code replicas,

15 combining and accumulating the mixed incoming and PRN code replicas, thereby obtaining a correlation signal, and

using the correlation signal to adjust the phase of the locally generated PRN code replicas with respect to the PRN code of the incoming signal in order
20 to maximize the correlation, thereby to lock the phase of the locally generated PRN code replicas to the phase of the PRN code in the incoming signal.

17. The method of claim 16, wherein K equals 10 and N equals 2.

18. The method of claim 16, wherein mixing the incoming signal with the first, second, third and fourth locally generated PRN code replicas results in corresponding first, second, third and fourth mixed
5 signals, and wherein combining and accumulating said mixed signals includes giving the first and fourth mixed signals the same polarity that is different from a common polarity of the second and third mixed signals.

19. The method of claim 18, wherein the combining and accumulating of said mixed signals is performed by first doing the accumulating and then doing the combining.

20. The method of claim 18, wherein the combining and accumulating of said mixed signals is performed by doing at least some of the combining before the accumulating.

21. A receiver of a composite radio frequency signal including a plurality of signals that individually include a carrier signal having encoded thereon a pseudo-random noise (PRN) binary code,
5 comprising:

means receiving the composite radio frequency signal for transforming the composite signal into an intermediate frequency signal, whereby the intermediate frequency signal includes a plurality of signals that
10 individually include an intermediate frequency carrier signal having the PRN code encoded thereon,

a plurality of channel circuits receiving the intermediate frequency signal, individual ones of said plurality of channel circuits including means for
15 decoding one of the plurality of intermediate frequency signals that comprises:

means responsive to an error signal for locally generating a PRN signal corresponding to the PRN code of the intermediate frequency signal with a relative phase controlled by a
20 magnitude of the error signal,

means for mixing the locally generated PRN signal with the intermediate frequency signal,

25 means using the mixed signal for generating an error signal having a magnitude

as a function of a relative phase difference between the PRN code of one of the intermediate frequency signals and the locally generated PRN signal that (a) is zero for a zero relative phase difference and for a majority of a range of the relative phase difference between plus and minus one chip, and (b) increases as the relative phase difference changes from zero to another value within a central portion of said range.

22. The receiver of claim 21 wherein the local PRN signal generating means includes means for generating an operating set of recurring non-zero gating signals representing edges of the PRN code and which individually (a) are less than one chip in duration, (b) have equal positive and negative areas, and (c) have a positive or negative polarity at a center thereof corresponding to whether a PRN code edge is positive or negative going.

23. The receiver of claim 22 wherein the local PRN signal generating means additionally includes means for generating an initial set of non-zero recurring gating signals that individually (i) are less than one chip in duration, and (ii) have a single positive or negative polarity that designates whether a PRN code edge is respectively positive or negative going, and wherein individual ones of the plurality of channel circuits includes means for selecting one of the operating or initial set of gating signals for mixing by the mixing means with the intermediate frequency signal.

24. The receiver of claim 21 wherein the local PRN signal generating means includes means for generating an operating set of PRN signals that includes

5 a first replica advanced in phase $1/2K$ of said chip with
respect to a reference and with a first polarity, a
second replica delayed in phase $1/2K$ of said chip with
respect to said reference and having a second polarity
opposite to the first polarity, a third replica advanced
10 in phase $N/2K$ of said chip with respect to said
reference and with said first polarity, and a forth
replica delayed in phase $N/2K$ of said chip with respect
to said reference and with said second polarity, wherein
N and K are integers with N being smaller than K.

25. The receiver of claim 24, wherein K
equals 10 and N equals 2.

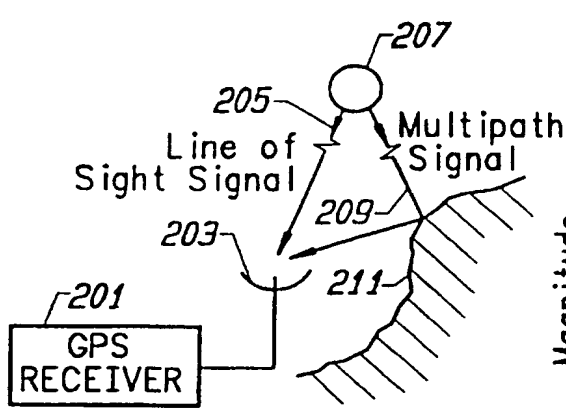


FIG. 1

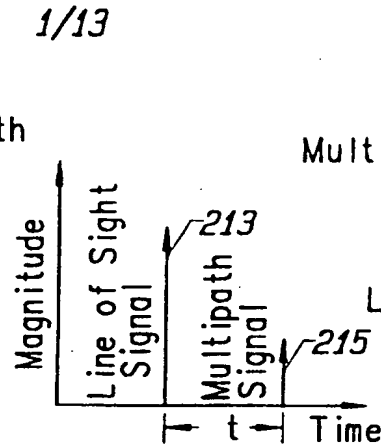


FIG. 2

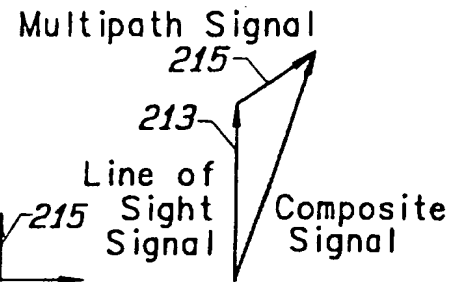


FIG. 3

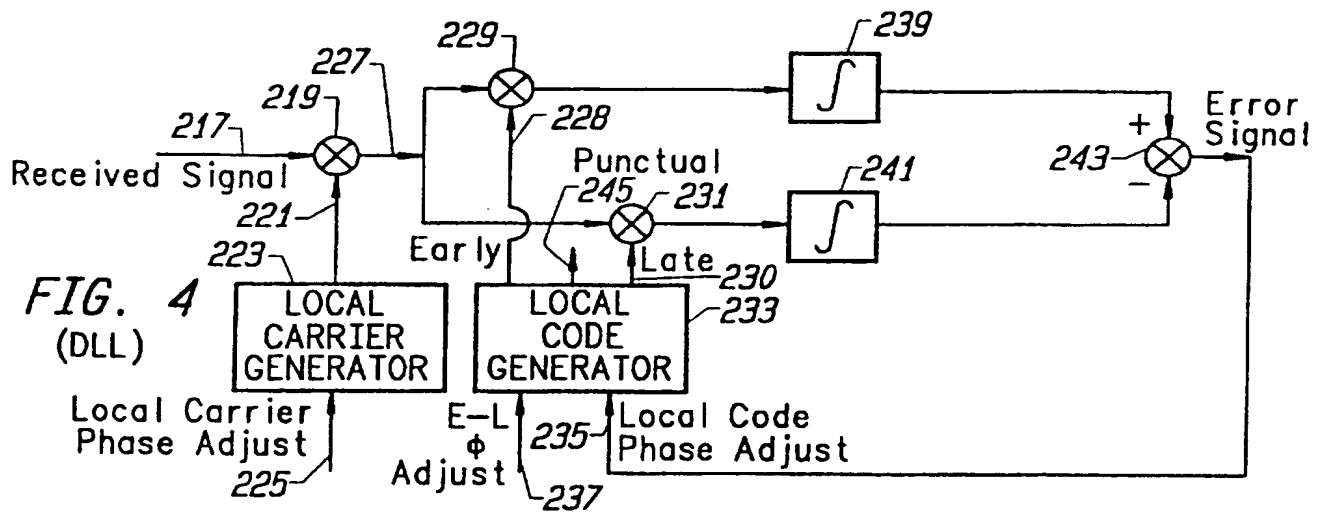


FIG. 4
(DLL)

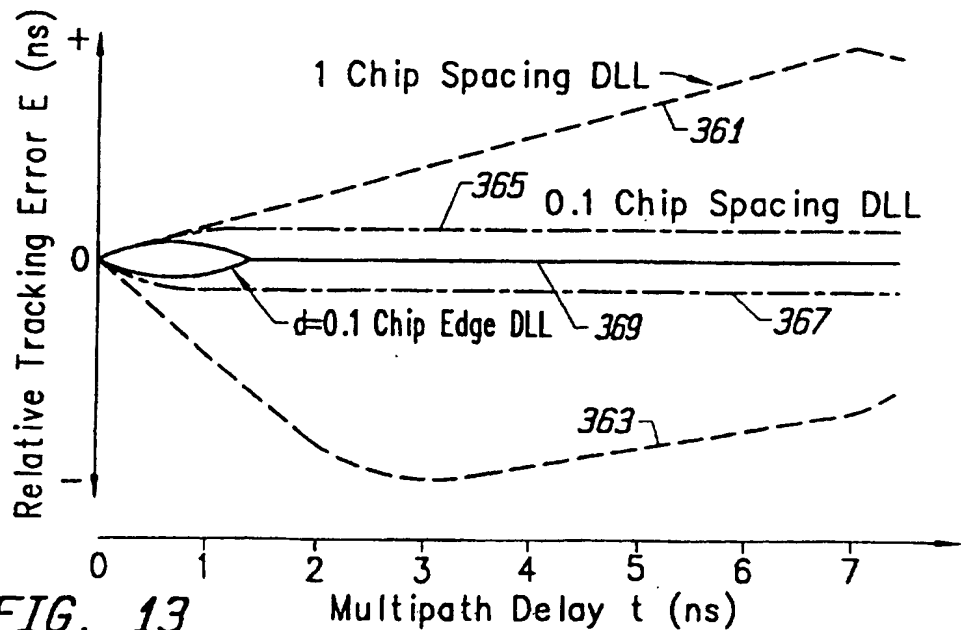


FIG. 13

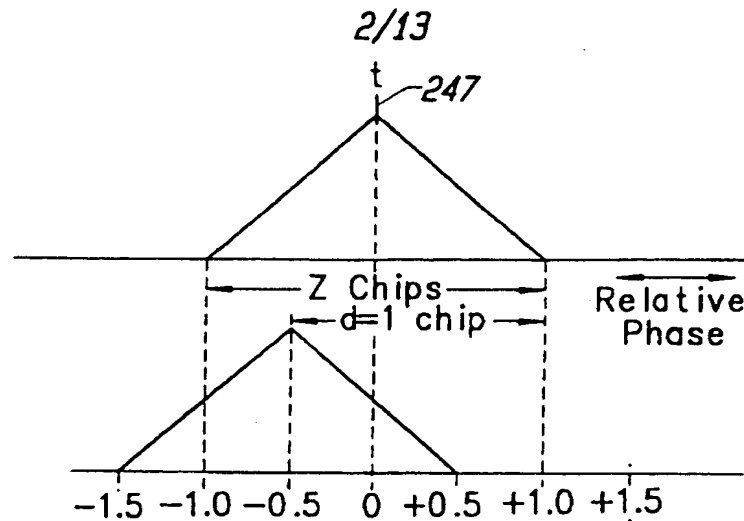


FIG. 5A
(Punctual)

FIG. 5B
(Early)

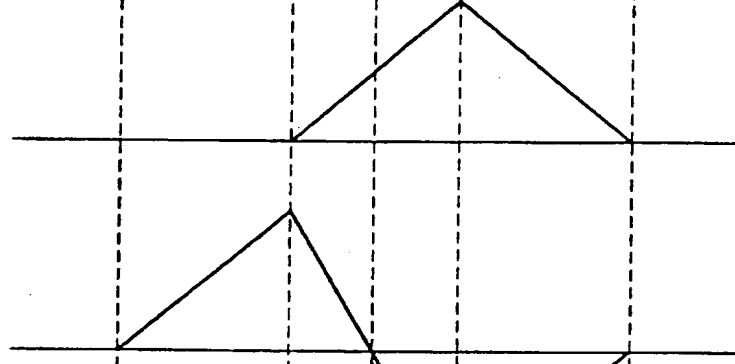


FIG. 5C
(Late)

FIG. 5D
(Error Signal)

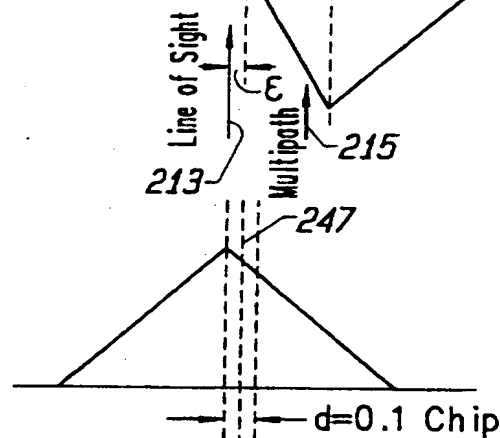


FIG. 6A
(Early)

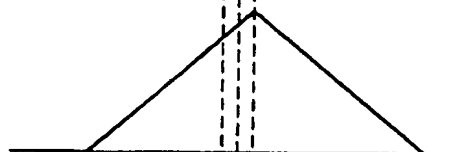


FIG. 6B
(Late)

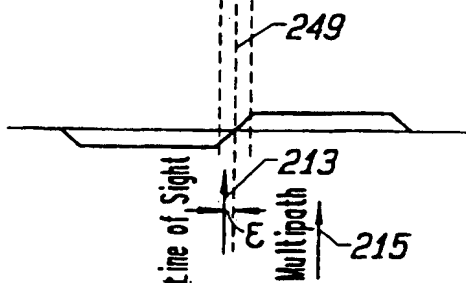


FIG. 6C
(Error Signal)

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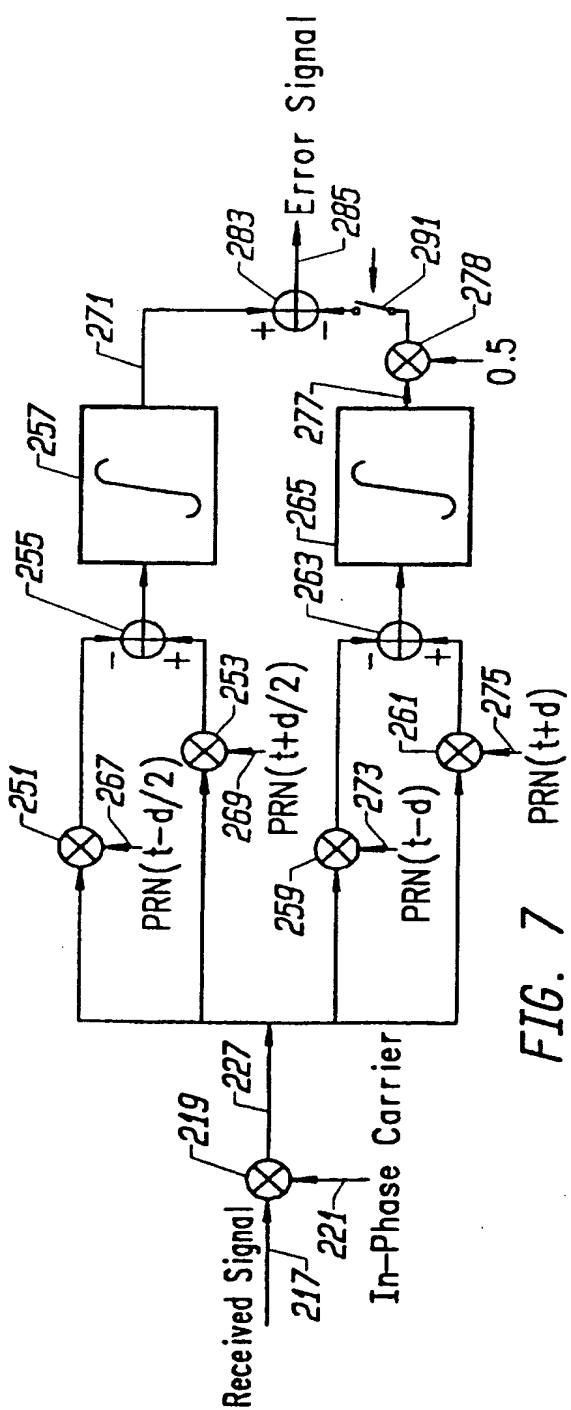


FIG. 7

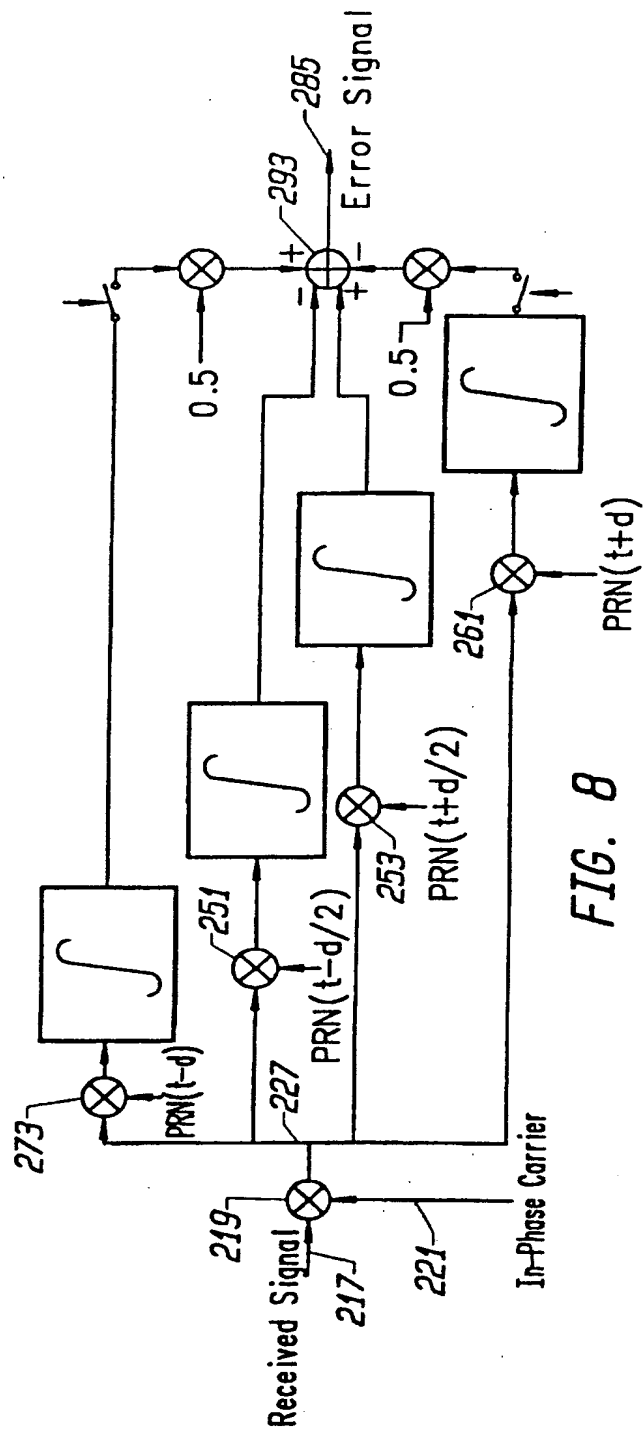


FIG. 8

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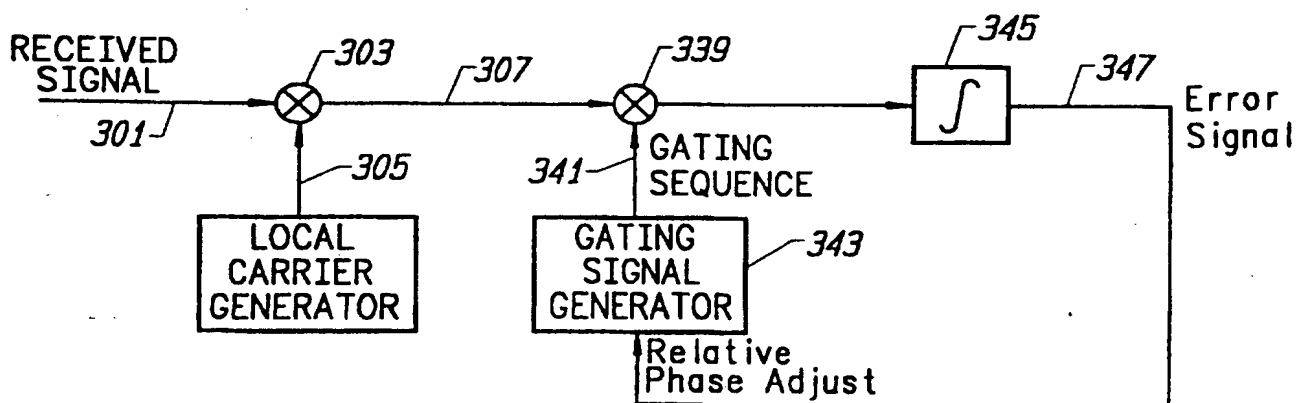
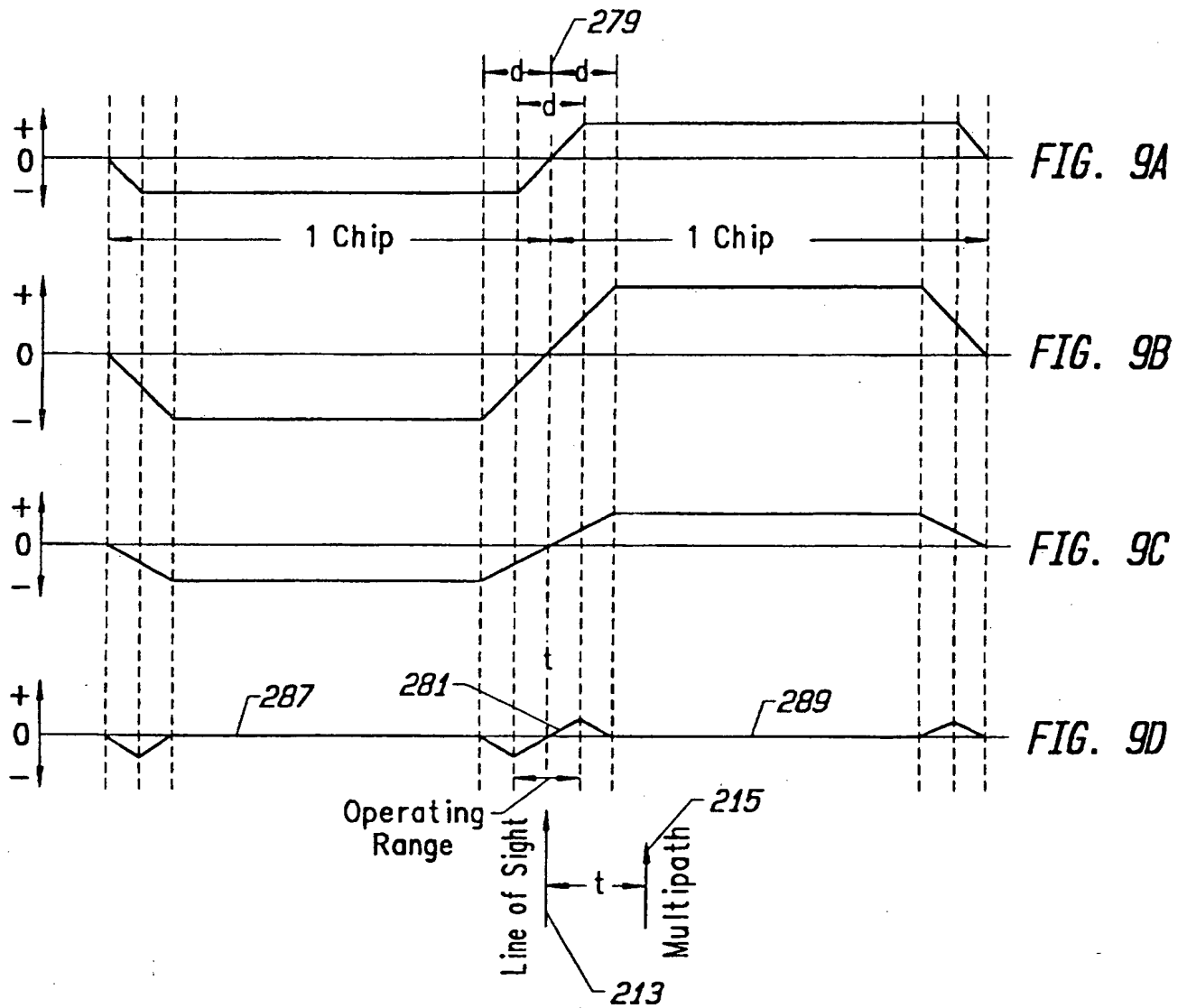


FIG. 10
SUBSTITUTE SHEET (RULE 26)

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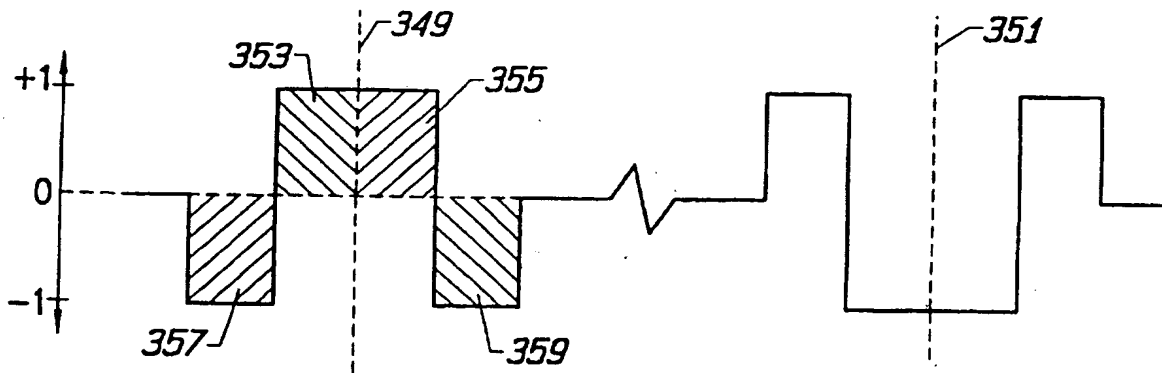
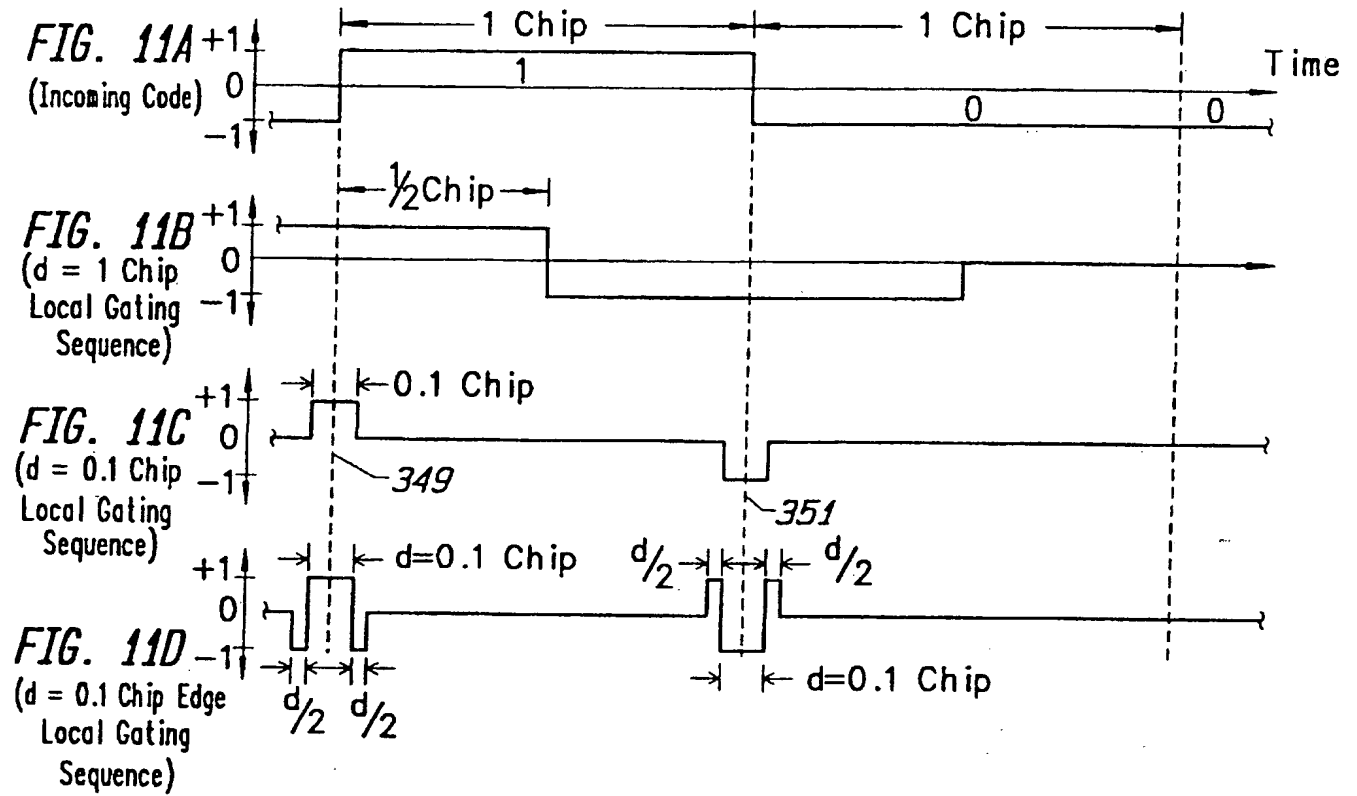


FIG. 12

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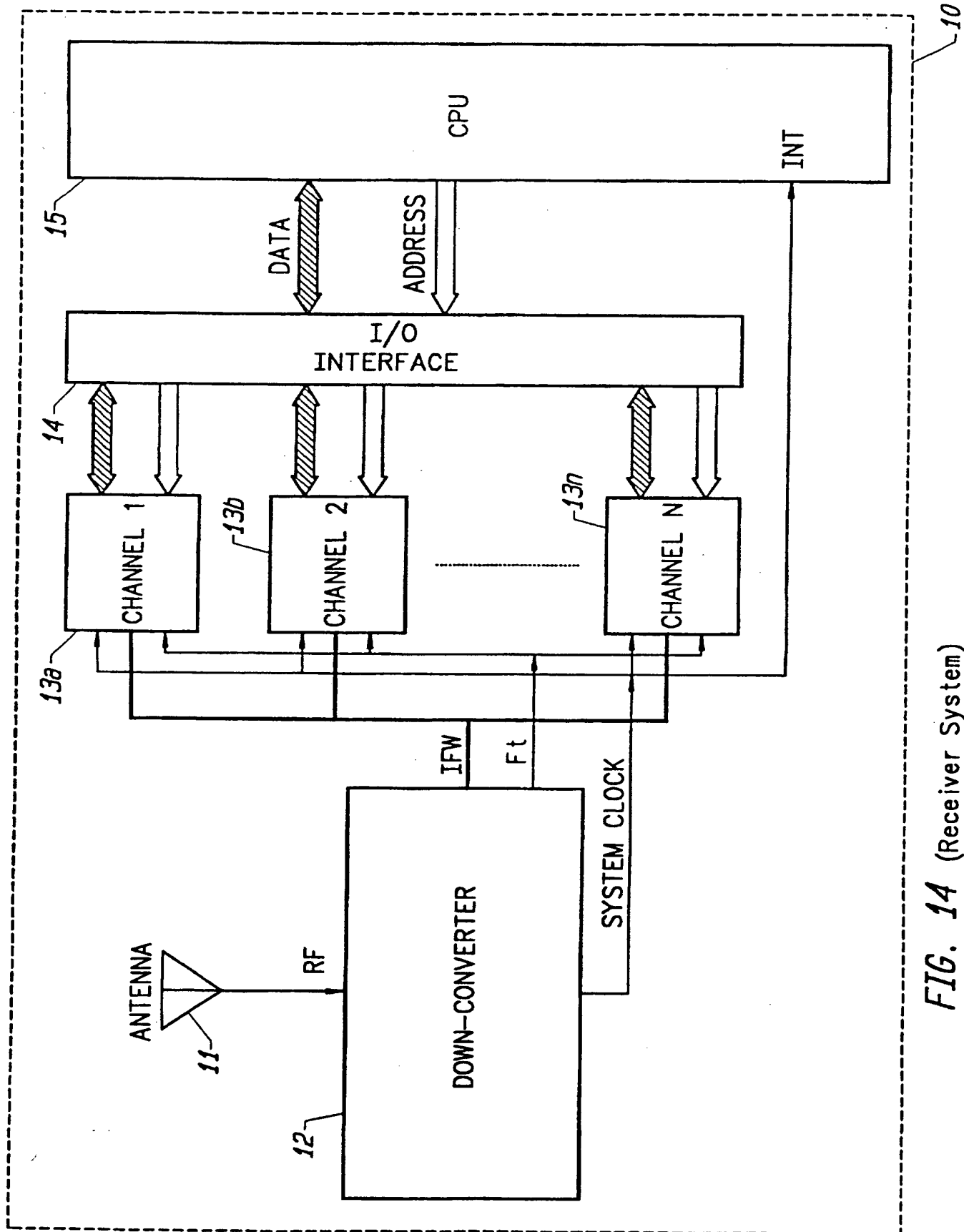
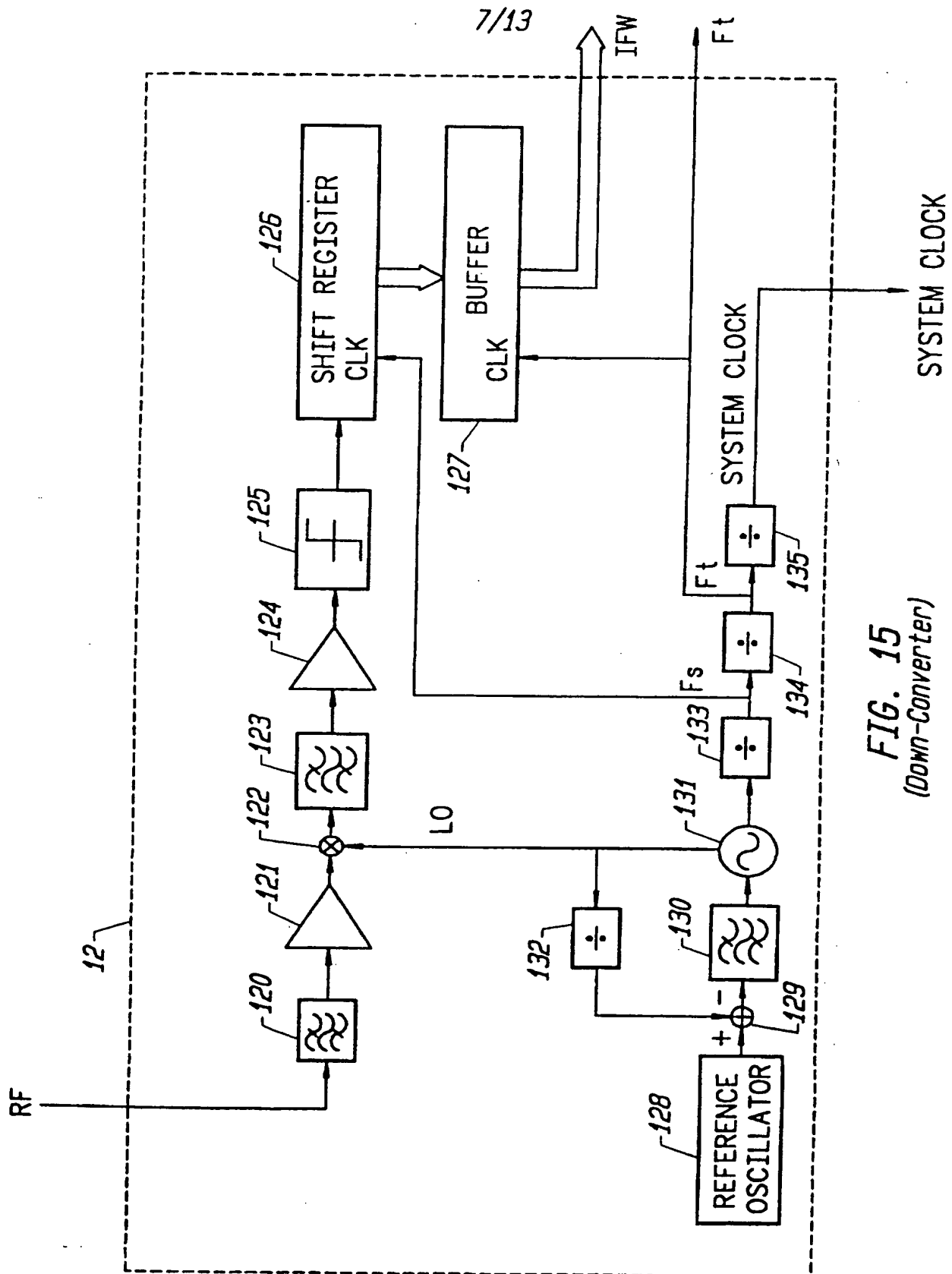
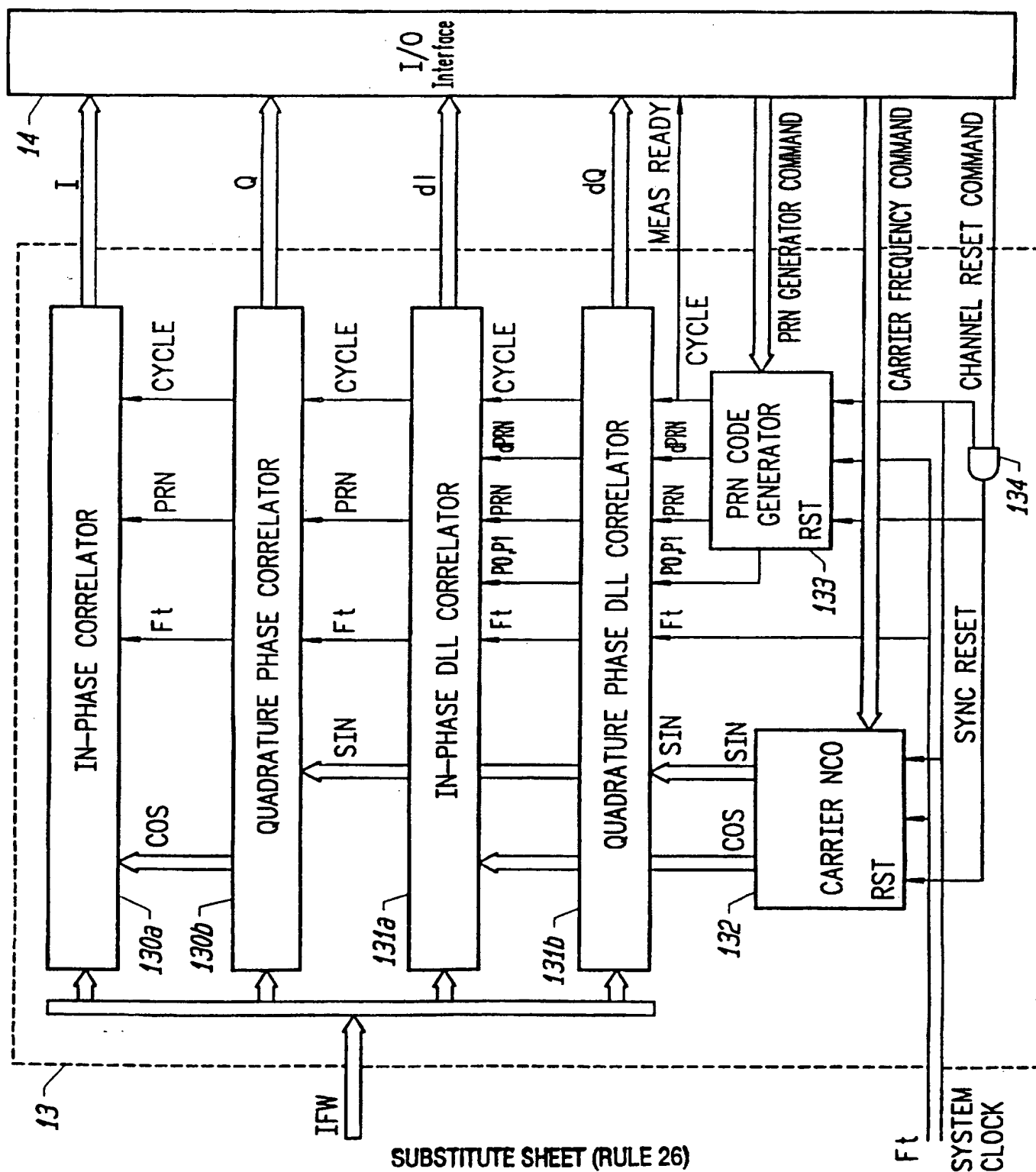


FIG. 14 (Receiver System)



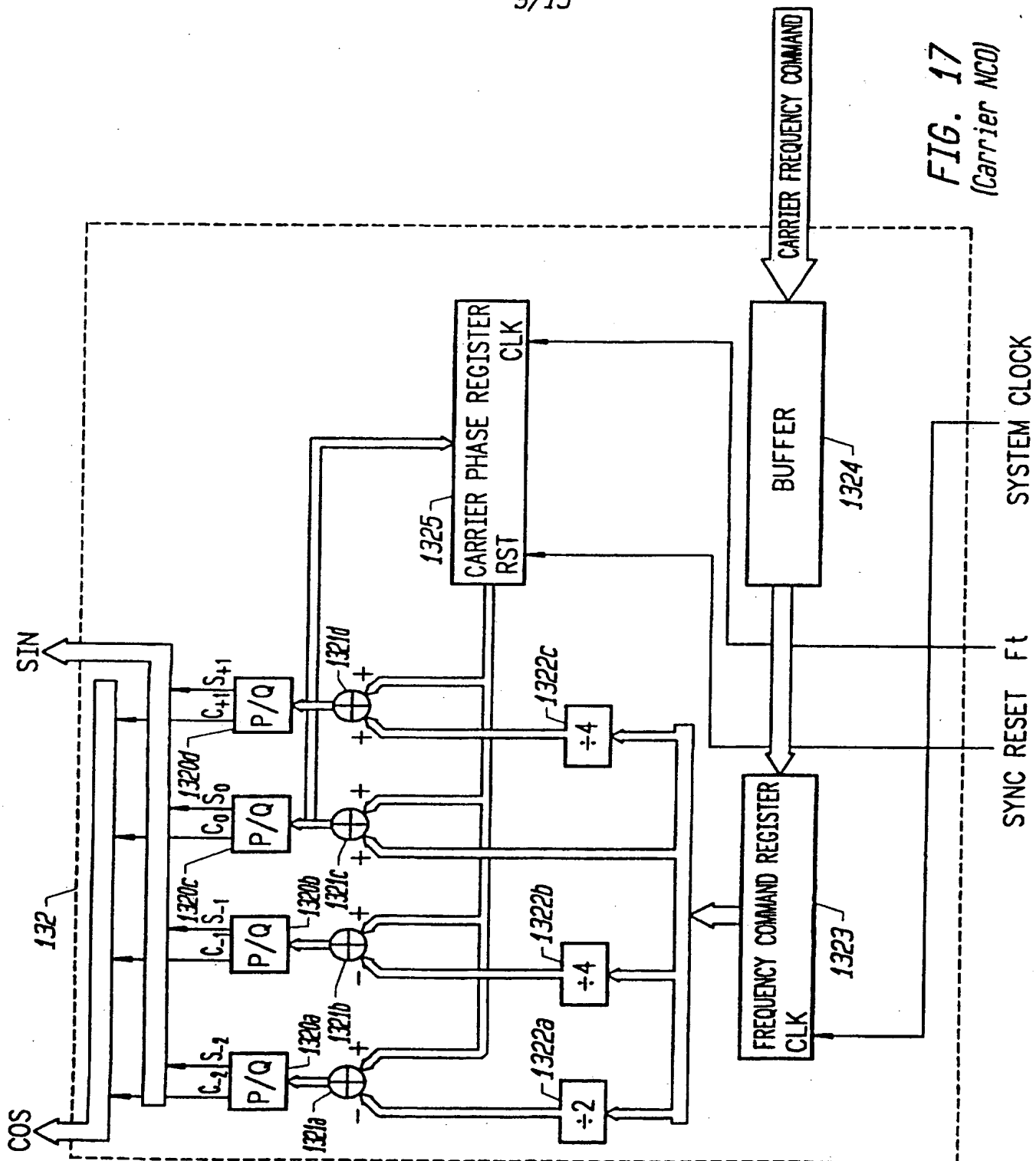
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FIG. 16
(One Channel)

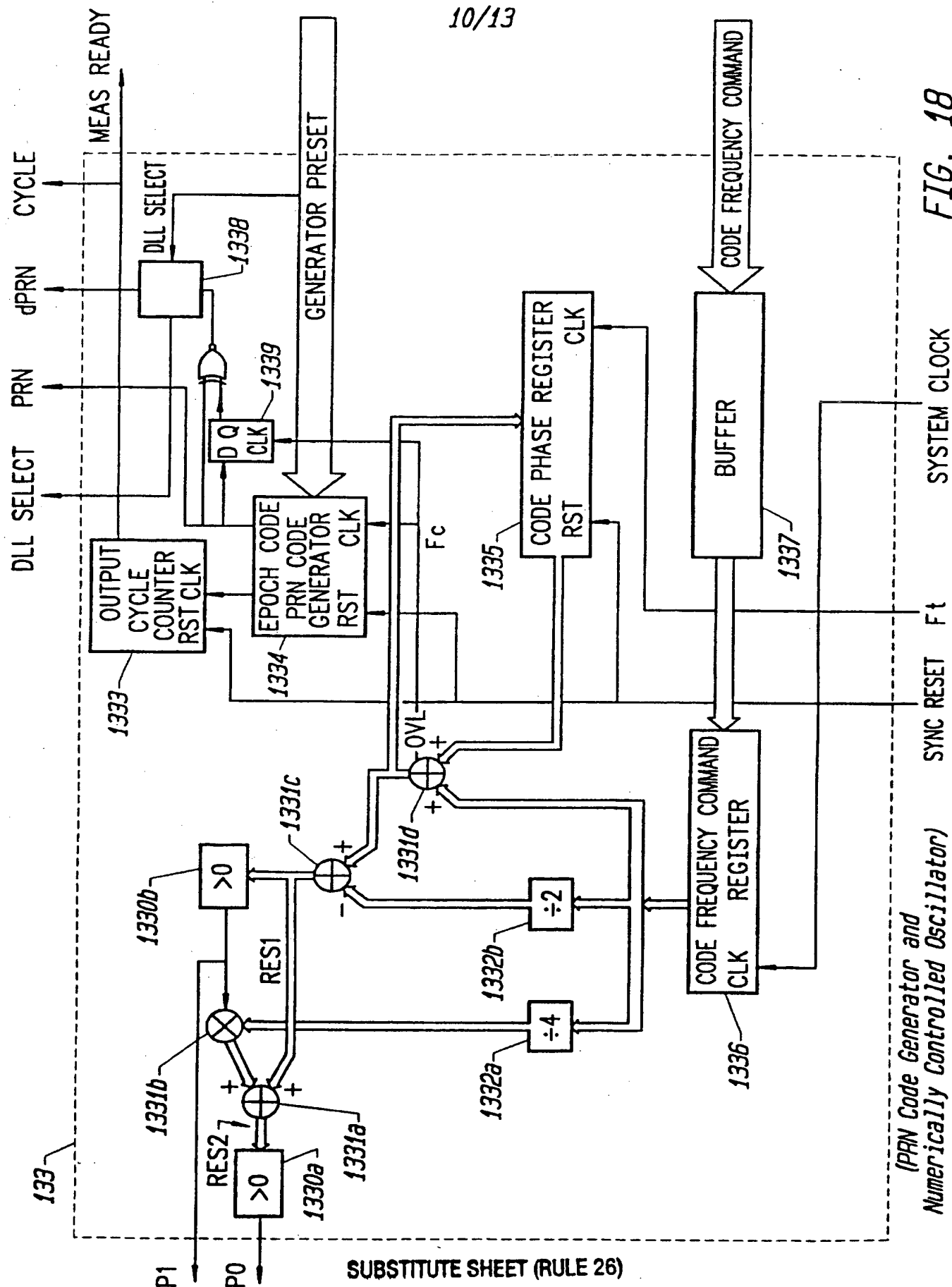


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FIG. 17
(Carrier NCO)



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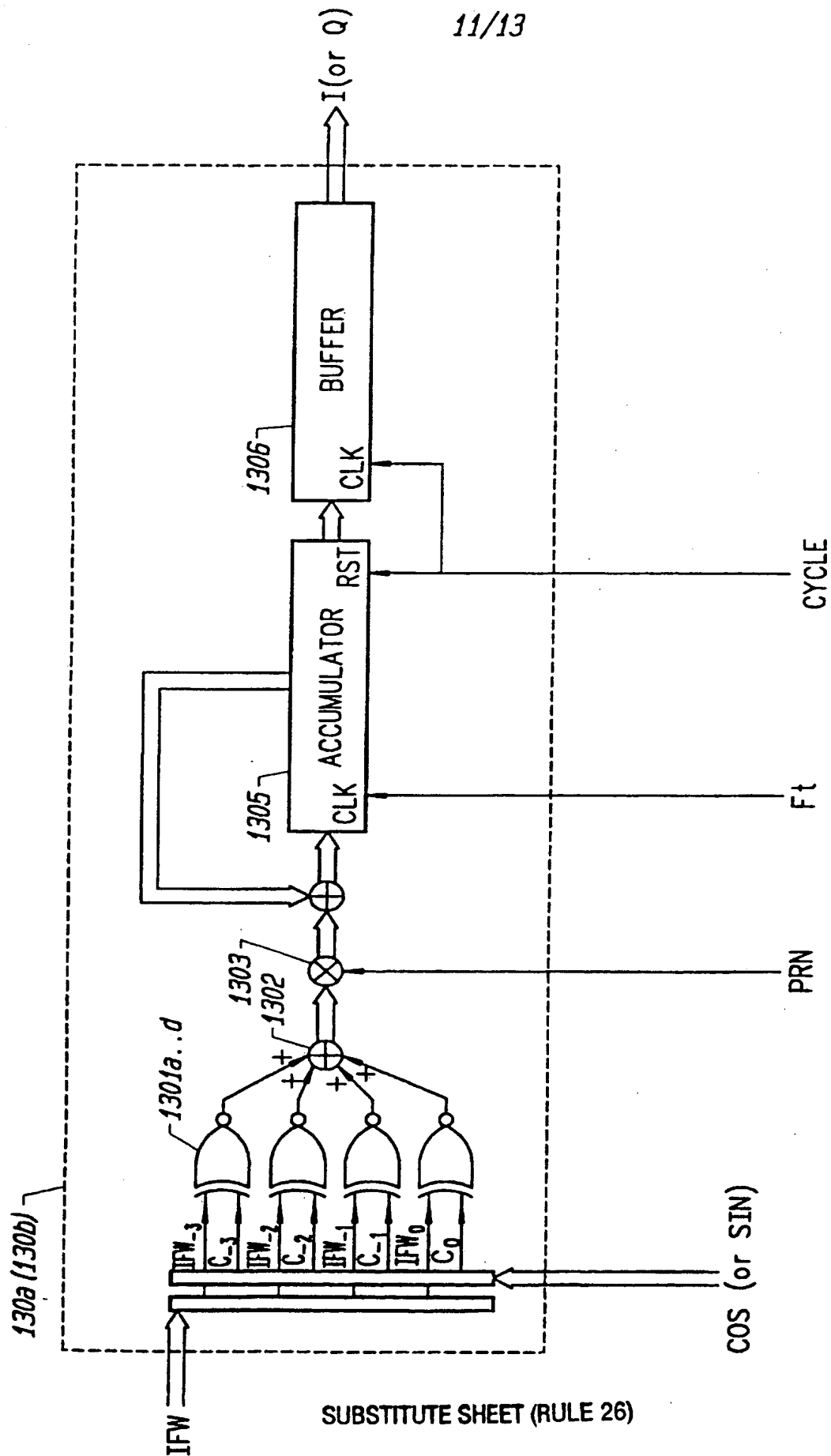


FIG. 19
(Correlator)

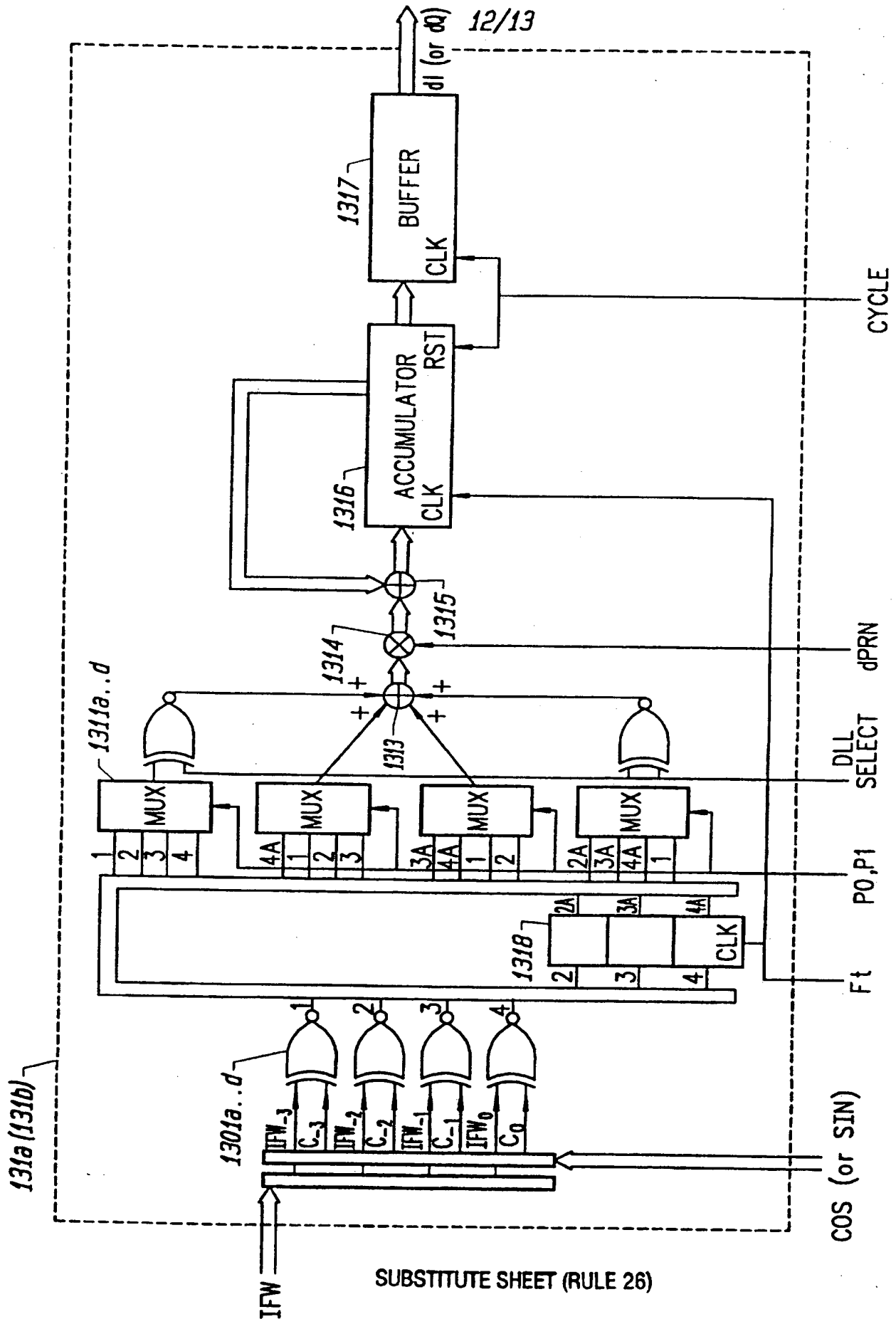


FIG. 20

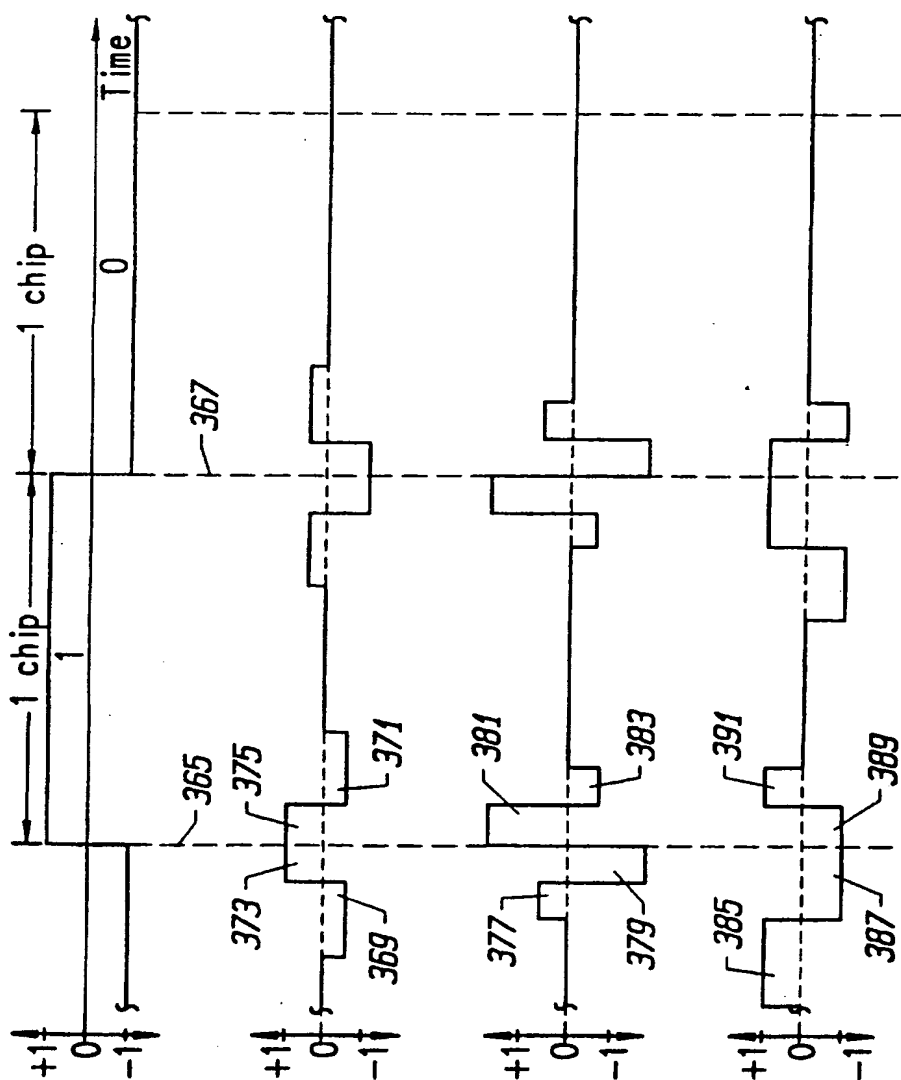
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FIG. 21A
(Incoming Code)

FIG. 21B

FIG. 21C

FIG. 21D



INTERNATIONAL SEARCH REPORT

Int'l Application No

PCT/US 96/12967

A. CLASSIFICATION OF SUBJECT MATTER
 IPC 6 G01S1/04 H04B1/707

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 6 G01S H04B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A E A	<p>EP 0 552 975 A (NOVATEL COMMUNICATIONS LTD) 28 July 1993 see page 3, line 19 - line 34 see page 7, line 54 - line 57 --- WO 96 37789 A (LEICA INC ; STANSELL THOMAS ATLEE JR (US); KNIGHT JERRY EUGENE (US)) 28 November 1996 see page 37, line 4 - page 38, line 24; figure 4 see page 44, line 25 - page 46, line 23; figures 23-25 --- US 5 347 536 A (MEEHAN THOMAS K) 13 September 1994 see the whole document --- -/-</p>	<p>9 1,13,16, 21 1-3, 8-10, 13-15, 21-23 1,9,13, 16,21</p>

☒ Further documents are listed in the continuation of box C.

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Date of the actual completion of the international search

17 March 1997

Date of mailing of the international search report

27.03.97

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INTERNATIONAL SEARCH REPORT

Int. Patent Application No.

PCT/US 96/12967

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A	EP 0 590 298 A (ASCOM TECH AG) 6 April 1994 see the whole document -----	1,9,13, 16,21

INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

PCT/US 96/12967

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